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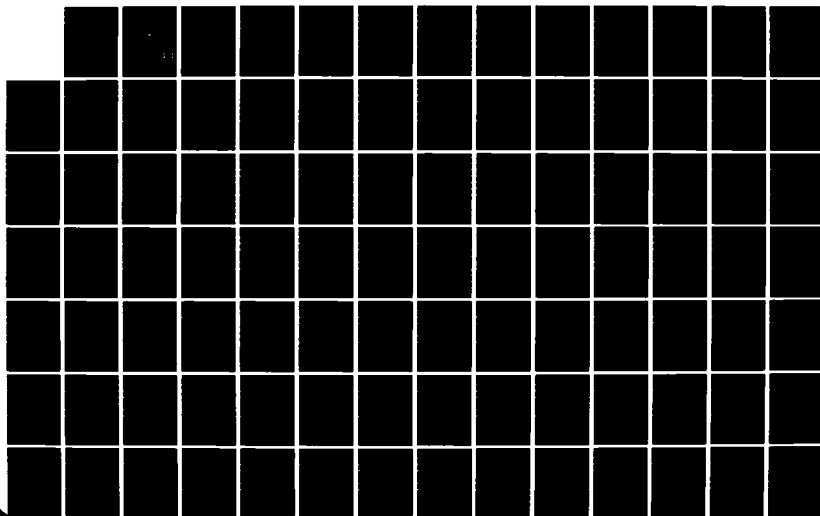
PRELIMINARY HELICOPTER DESIGN DECISION MAKING BASED ON  
FLIGHT PERFORMANCE FACTORS(U) NAVAL POSTGRADUATE SCHOOL  
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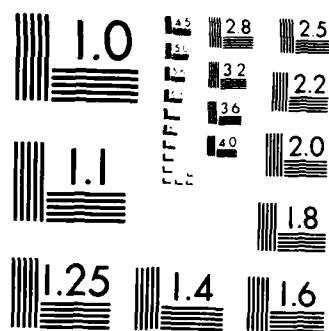
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NAVAL POSTGRADUATE SCHOOL  
Monterey, California



THESIS

PRELIMINARY HELICOPTER DESIGN DECISION  
MAKING BASED ON FLIGHT PERFORMANCE FACTORS

by

Patrick V. Adamcik

September 1984

Thesis Advisor:

Donald M. Layton

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## 20. ABSTRACT (Continue on reverse side if necessary and identify by block number)

This thesis will assist those evaluating helicopter design to make preliminary judgments about the feasibility of new designs. By using the computer program developed in this thesis, a designer can produce estimates for power requirements, endurance velocity, rate of climb, range velocity, hover ceiling, and service ceiling versus main rotor radius. These

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estimates can also be examined for the effects of changes in main rotor radius, chord, and rotational velocity.

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Preliminary Helicopter Design Decision Making Based  
on Flight Performance Factors

by

Patrick V. Adamcik  
Captain, United States Army  
B.S., University of Texas at Austin, 1977

Submitted in partial fulfillment of the  
requirements for the degree of

MASTER OF SCIENCE IN AERONAUTICAL ENGINEERING

from the

NAVAL POSTGRADUATE SCHOOL  
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## ABSTRACT

This thesis will assist those evaluating helicopter design to make preliminary judgments about the feasibility of new designs. By using the computer program developed in this thesis, a designer can produce estimates for power requirements, endurance velocity, rate of climb, range velocity, hover ceiling, and service ceiling versus main rotor radius. These estimates can also be examined for the effects of changes in main rotor radius, chord, and rotational velocity.

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## I. INTRODUCTION

A military engineering officer in a program or project office would probably never be called on to prepare a conceptual design of a helicopter, but he may well be required to evaluate a proposal submitted by a commercial contractor.

The requirement for such an evaluation might be stated as:

Determine if this design meets or exceeds the performance factors listed on the next page and if the design can be changed to optimize the performance.

There are several approaches one could use to complete this task. One could use a hand held calculator and enter the data for the many equations, or one could write a program for a micro or main frame computer to produce the required information. Both these options are laborious and time-consuming. By choosing the first option, one may be able to complete the task in two or three weeks or if it is decided to write a program, one may finish in one week provided that there are no "bugs".

The best solution of course, is to use an existing program which can determine the necessary information for the specification parameters. In addition, this program should be able to show what happens if certain parameters

are allowed to vary, thus providing the formation for optimization.

The objective of this thesis was to develop such a program that will graphically represent power requirements, endurance velocity, rate of climb, range velocity, hover ceiling and service ceiling all as a function of main rotor radius for four different cases. The graphs that result from this program should enable one not only to evaluate the basic helicopter design, but also to make recommendations for design improvement.

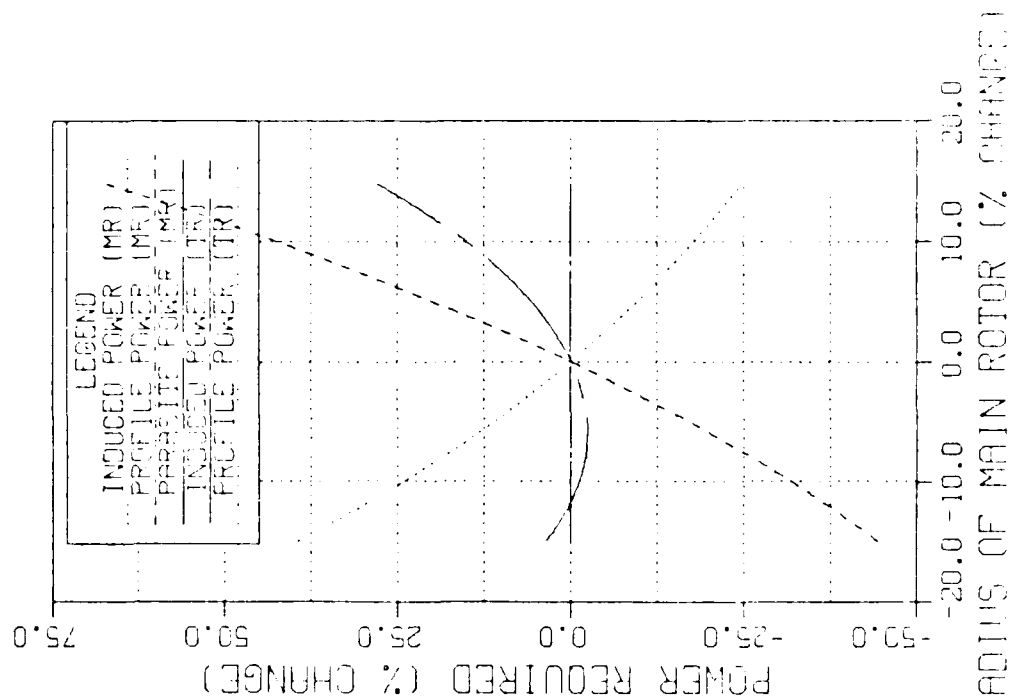
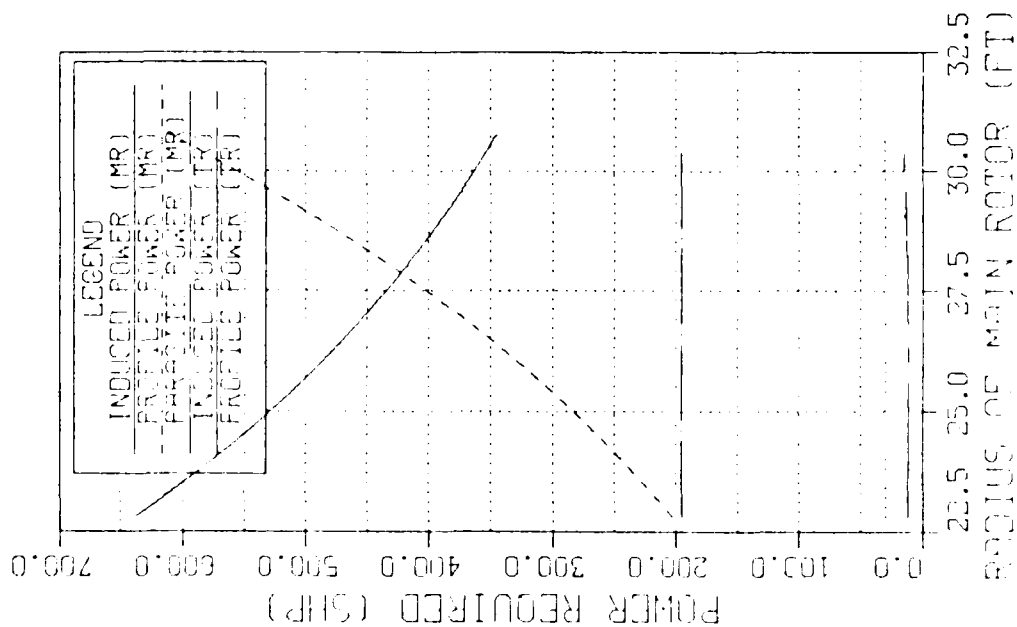
## II. APPROACH TO THE PROBLEM

Six performance factors (power requirements, endurance, velocity, rate of climb, range velocity, hover ceiling and service ceiling) were determined to be major in designing of a helicopter. In order to obtain estimates for these, a Fortran program was to be written to be used with "DISSELA" (Display Integrated Software System and Plotting Language). [Ref. 1], to plot the results of the performance factors versus main rotor radius on either a screen or as a hard copy from the main frame computer.

The equations required for calculating these factors were obtained from "Helicopter Performance", [Ref. 2], and "Helicopter Design Manual", [Ref. 3], both written by Donald M. Layton. These equations were examined and then grouped for the purpose of writing subroutines to ensure an effective use of computer time. The result was six subroutines, Sub-group A, [Appendix B], are used in all the performance calculations. Sub-group A consist of:

1. RHO - Calculates density from pressure altitude and temperature or given density altitude. Also determines pressure and temperature ratio for altitude versus sea level.
2. VELMR - Calculates induced velocity for main rotor.
3. VELTR - Calculates induced velocity for tail rotor.

# POWER VERSUS RADIUS CHORD & ROTATIONAL VELOCITY HELD CONSTANT SOLIDITY, TIP VELOCITY & ADVANCE RATIO ALLOWED TO VARY WITH RADIUS



## APPENDIX A

### COMPUTER PROGRAM OUTPUT - PLOTS

## V. CONCLUSIONS

The objective of this thesis to design a program that evaluates a given set of helicopter design values was accomplished. The program will generate thirty two (32) graphs of six (6) performance factors for any single-rotor helicopter. The program does allow for one to optimize a design through the evaluation of the variation of parameters for each performance factor.

At this point, the program takes into account neither compressibility nor blade stall. These factors would improve the estimations and may prove to be a worthwhile project for further work. Other points which could be examined are twin-blade and no-tail-rotor helicopters. Of the points mentioned above, blade design would probably be of most importance since little has been done to examine the optimization of blade twist and composite structure of blades.



MAXIMUM RATE OF CLIMB VERSUS RADIUS CHANGE  
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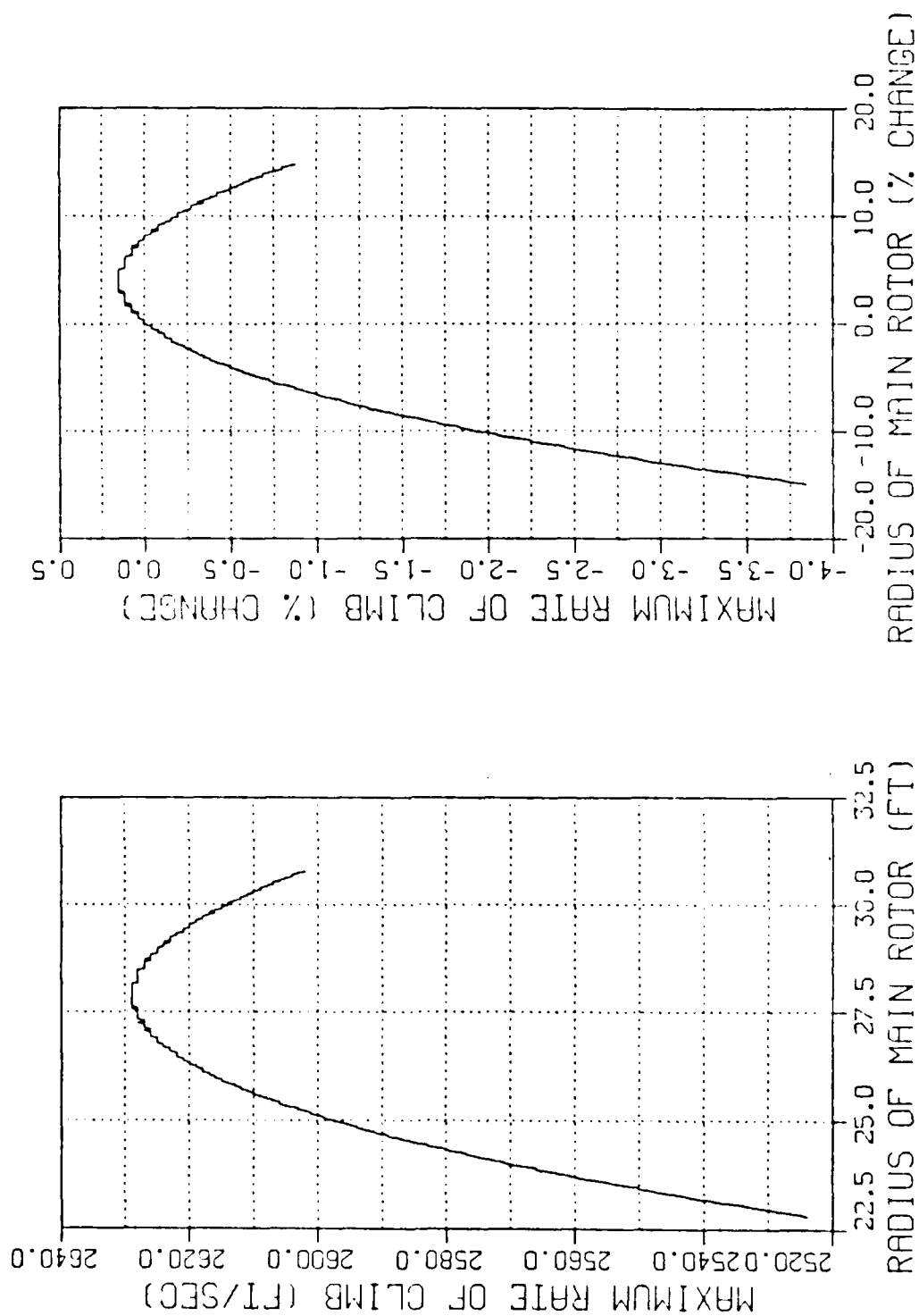


Figure 4.4 Example Maximum Rate of Climb - Case 4

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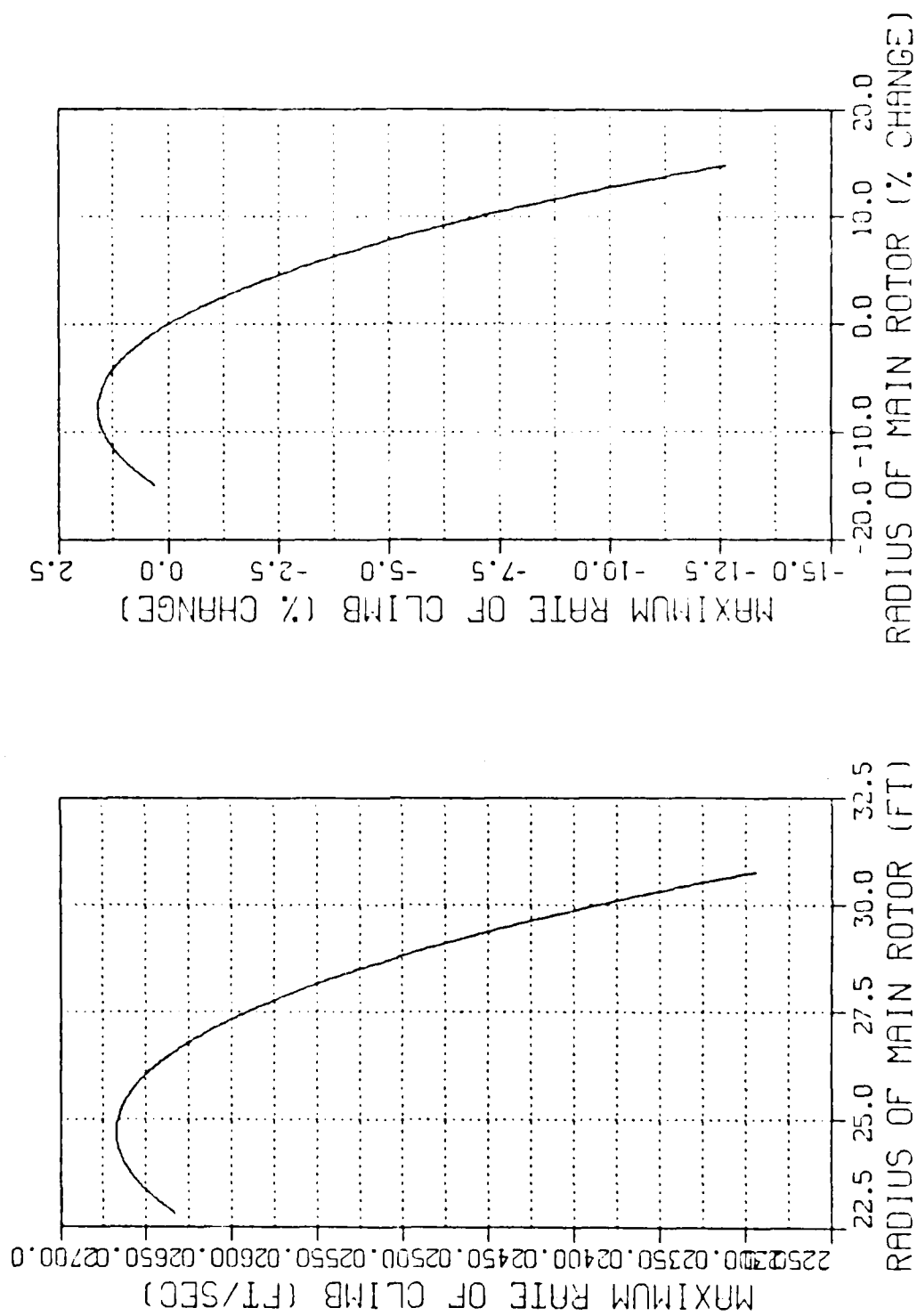


Figure 4.3 Example Maximum Rate of Climb - Case 3

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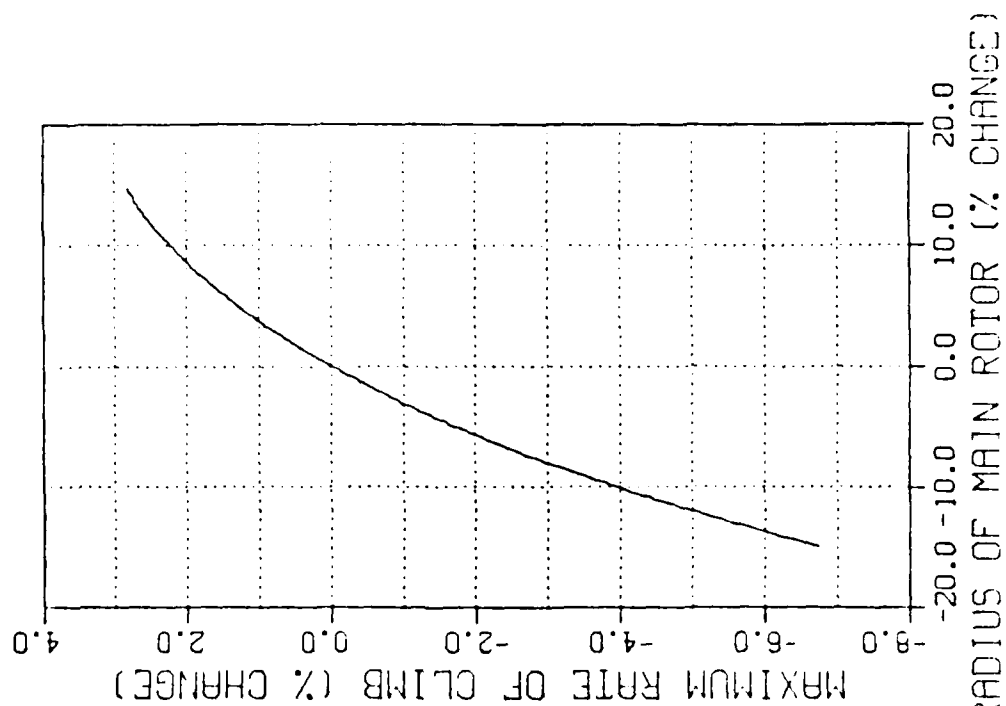
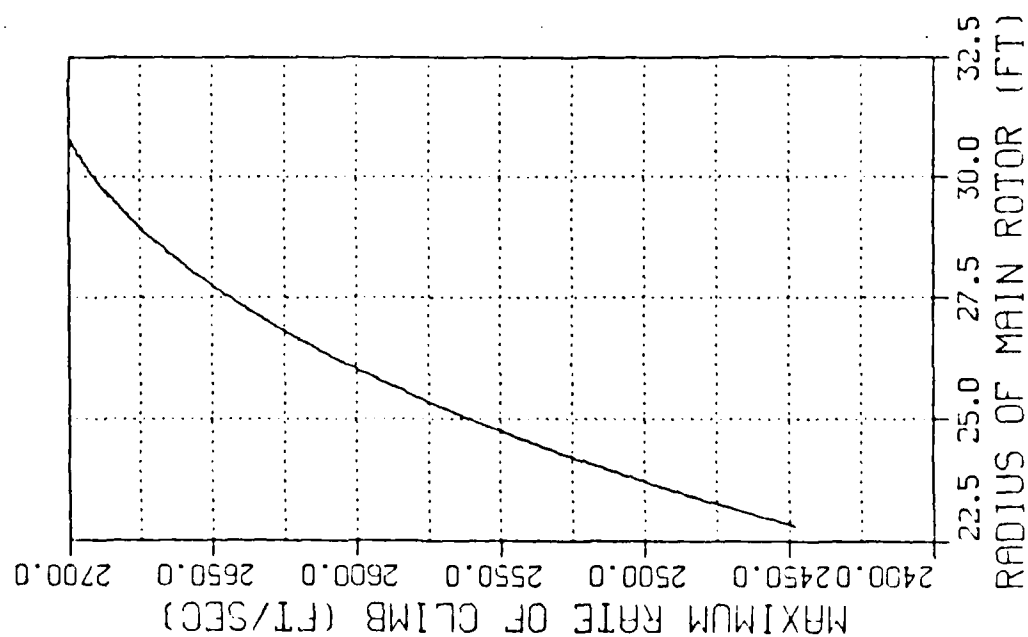


Figure 4.2 Example Maximum Rate of Climb - Case 2

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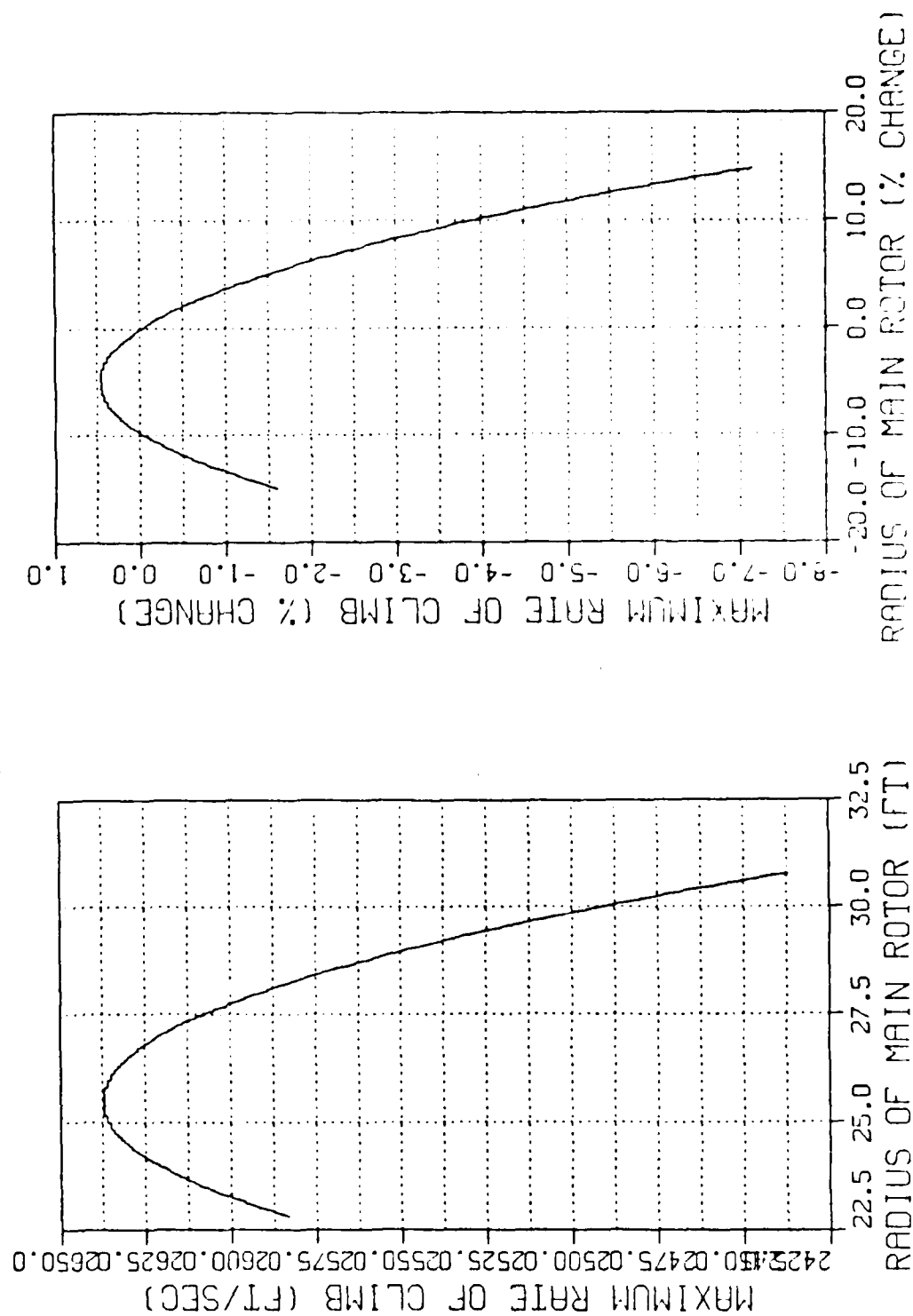


Figure 4.1 Example Maximum Rate of Climb - Case 1

and percent increase of rate of climb. The cases were explained in Table 3 and the Figures follow Table 4.

Table 4

Case Evaluation of Maximum Rate of Climb Plots

Case	Figure Reference	Rate of Climb(ft/sec)	Radius (ft)	Percent Increase
1	4.1	2628	27.8	+ 0.130
2	4.2	2668	24.8	- 0.156
3	4.3	2700	30.63	+ 2.80
4	4.4	2637	25.63	- 5.00

From examining Table 4, it would be best to increase the radius to 30.63 feet while holding the chord to 1.75 feet, the tip velocity to 723.6 ft/sec (radius times rotational velocity), changing the rotational velocity to 23.62 rad/sec, and calculating solidity from radius and chord. This, however, may not be the best answer if there is a limitation to the radius of the blade. For this particular example, the optimum solution may be to leave the design as it is. Increasing or decreasing the radius by small amounts does little to increase or decrease the rate of climb.

One must not only look at one factor in making the final decision. The changes affect the performance factors in different ways, therefore, the final decision must be made after weighting all the changes against all the performance factors.

#### IV. RESULTS

The program will generate a total of thirty two (32) plots. The first twelve (12) pertain to power requirements. This includes induced, profile, and parasite power for the main rotor; and induced and profile power for the tail rotor. To indicate a relation between the power terms of the main rotor the figure of merit (induced divided by the sum of the induced and profile power) is included. The sum of the terms (total power) for the main and tail rotor was included with the total power required for the aircraft. The remaining twenty (20) plots are for the performance factors of endurance velocity, rate of climb, range velocity, hover ceiling and service ceiling.

The data for this particular model (UH-60A) was used to illustrate the features of the program and the results presented are typical for this example only. The specifications of any model or design can be used as long as the assumption of a single-mast helicopter with rectangular blades is followed.

The plots created by the program represent the results of varying the main rotor radius, chord or rotational velocity. To example how to interrupt the results, the four (4) plots for Maximum Rate of Climb will be analyzed. Table 4 compares the results in relation to rate of climb, radius

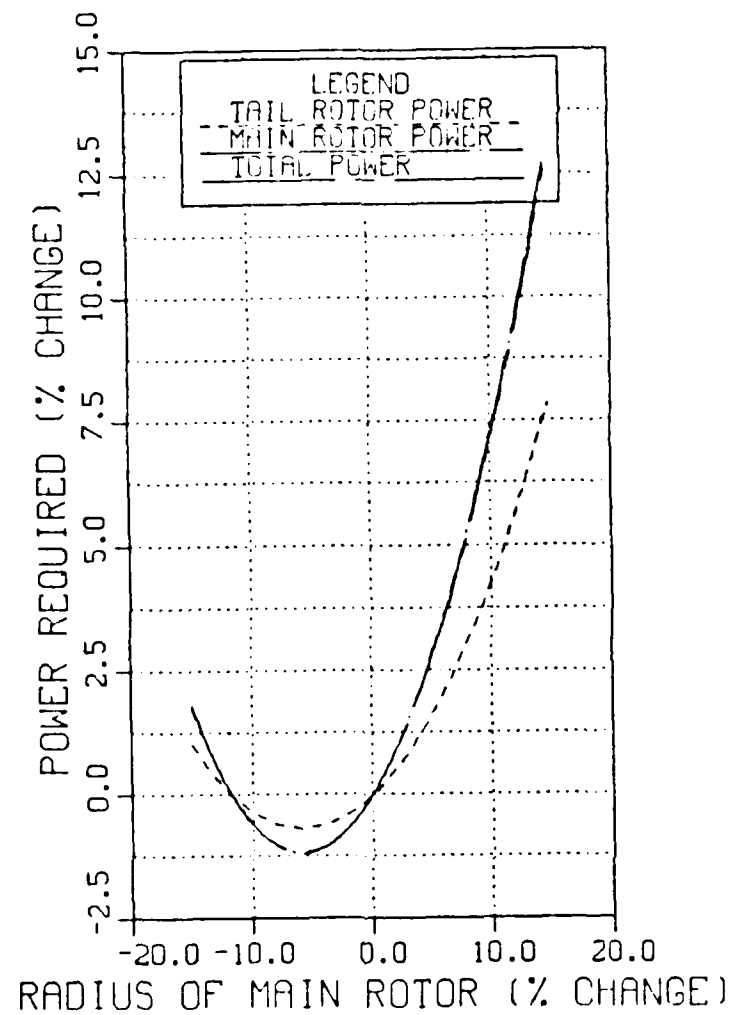


Figure 3.2 Example of Right Hand Plot

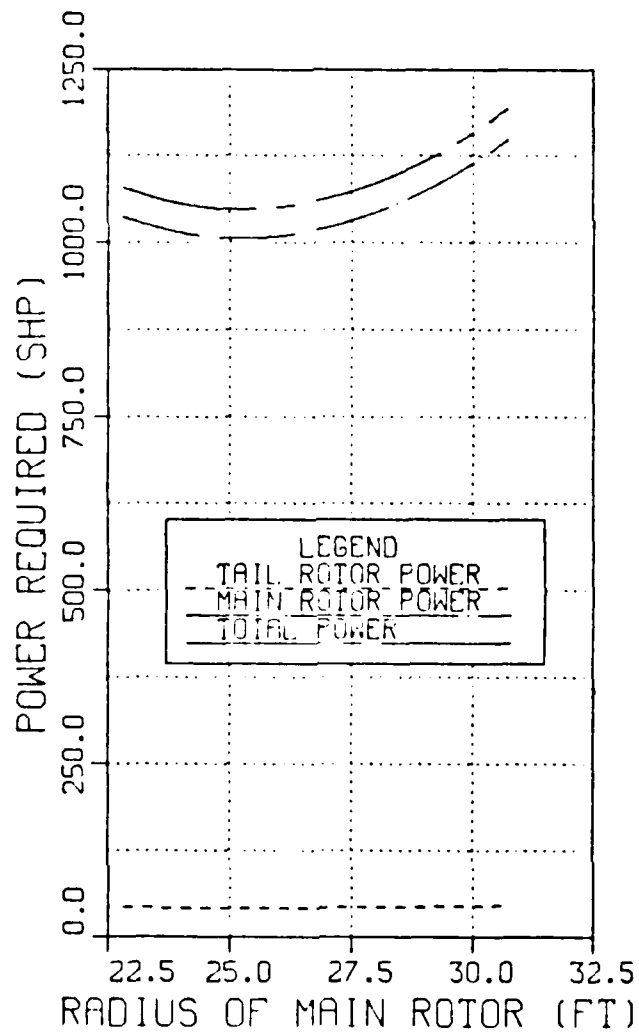


Figure 3.1 Example of Left Hand Plot

The right hand plot shows the values of the performance factors based on a percent difference from the value at the specification conditions versus a percent difference of the radius from the radius specification. Figure 3.2 shows an example of power required (% change) versus radius of the main rotor (% change), Case 1.



percent (3%) for transmission losses (if three engines are used, an additional transmission is required), [Ref. 2].

The secondary goal of the thesis was to examine four (4) different cases involving main rotor Radius, Chord, Rotational Velocity, Tip Velocity, Advance Ratio, and Solidity. Table 3 shows how these variables were used in each of the four (4) cases.

Table 3

Case Use of Variables

	Radius	Chord	Rotational Velocity	Advance Ratio	Tip Velocity	Solidity
Case 1	V	C	C	V	V	V
Case 2	V	C	V	C	C	V
Case 3	V	V	C	V	V	C
Case 4	V	V	V	C	C	C

V : VARIES      C : HELD CONSTANT

Advance Ratio, Tip Velocity, and Solidity when held constant keep their values at the specification conditions. The values of Chord and Rotational Velocity were allowed to vary when Advance Ratio, Tip Velocity, or Solidity were held constant as shown in Table 3.

The graphs consist of two (2) plots representing the same data but presented in different ways. The left hand plot shows the actual performance factor value versus main rotor radius. Figure 3.1 shows an example using power required versus main rotor radius, Case 1.

The example uses a value of four (4.0) feet. This value is assigned to a variable called "diff". The program was written to allow the X-axis scale of the plot to be adjusted in accordance with any value you might choose for "diff". The Y-axis scales can also change based on the maximum and minimum values for the performance factor being considered.

Certain assumptions had to be made in order to write the program. Table 2 lists these assumptions and factors used and the line number in the program where the factors can be changed if needed.

Table 2  
Assumptions Made in the Program

Assumption	Factor	Line Number
Single Mast Helicopters	NA	NA
Only Rectangular Blades	NA	NA
Profile Power Factor	4.3	1079,1108
Ground Effect Factor	1.6	1138
Transmission & Accessory Losses		
1 engine SHP = (# ENG*ESHP-10.0)*0.97		560,780.887
2 engines SHP = (# ENG*ESHP-10.0)*0.9*0.97		561,781.888
3 engines SHP = (# ENG*ESHP-10.0)*0.9*0.94		562,782.889

ENG: Engine, ESHP: Engine shaft horsepower,  
SHP: Rotor Shaft horsepower

The Transmission and Accessory Losses were calculated based on a loss of ten (10) horsepower for the accessories, ten percent (10%) for multiple engine installation, and three

### III. SOLUTION TO THE PROBLEM

The program requires input data prior to compiling and execution. To demonstrate how to use the program a set of sample data was used. Table 1 is a listing of the required input data for the program.

Table 1

#### Sample Data for Use in Program

	Main Rotor	Tail Rotor
Radius	26.8 ft	5.5 ft
Chord	1.75 ft	0.81 ft
Rotational velocity	27.0 rad/sec	124.6 rad/sec
Coefficient of drag	0.008	0.008
Number of blades	4	4

#### General Helicopter Data

Weight	20000.0 lbs
Tail boom length	31.5 ft
Effective flat plate area (forward)	25.7 sq ft
Effective flat plate area (vertical)	31.8 sq ft
Main rotor height above skids or wheels	11.2 ft
Aircraft velocity (power calculations only)	90.0 kts
Plus/minus (+/-) value for main rotor radius	4.0 ft

#### Engine Data

Number of engines	2
Shaft horsepower output (military)	1561.0 shp
Shaft horsepower output (normal)	1318.0 shp
Shaft horsepower output (cruise)	989.0 shp
Specific fuel consumption (military)	0.46 lbs/shp/hr
Specific fuel consumption (normal)	0.47 lbs/shp/hr
Specific fuel consumption (cruise)	0.51 lbs/shp/hr

As indicated in Table 1, a value is inputted for the range over which you wish to examine the main rotor radius.

4. POWMR - Calculates power requirements for main rotor only.

5. POWTR - Calculates power requirements for tail rotor and total aircraft.

6. CONST - Calculates general constants to be used in the first five subroutines listed above.

In addition to the subroutines listed above, six more, Sub-group B, [Appendix B], were written to perform the necessary iterations to calculate the performance factors. Some of Sub-group B subroutines were iterated in steps (1000,100,10,1) so that it would not require extensive computer time to obtain the desired results. A final eight subroutines, Sub-group C, [Appendix B], were written to plot the results using DISPLA.

The program takes into account neither compressibility nor blade stall. These considerations were omitted since this program was aimed at facilitating preliminary decision making for a new design, rather than a final production design, and usually the blade selected for a new design is taken from an existing helicopter.

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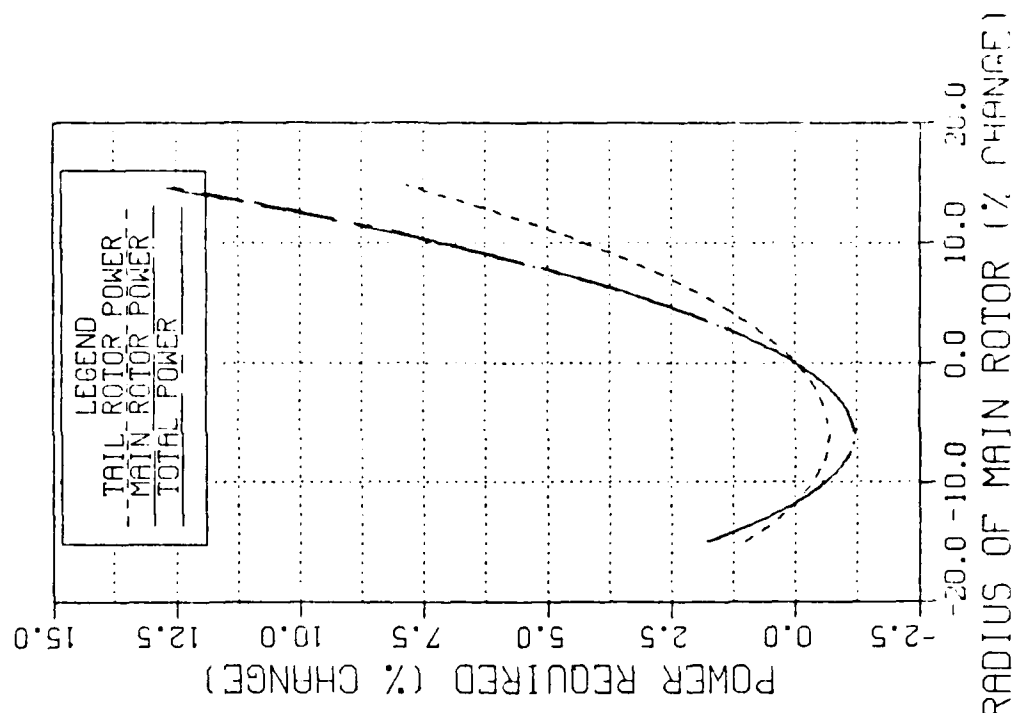
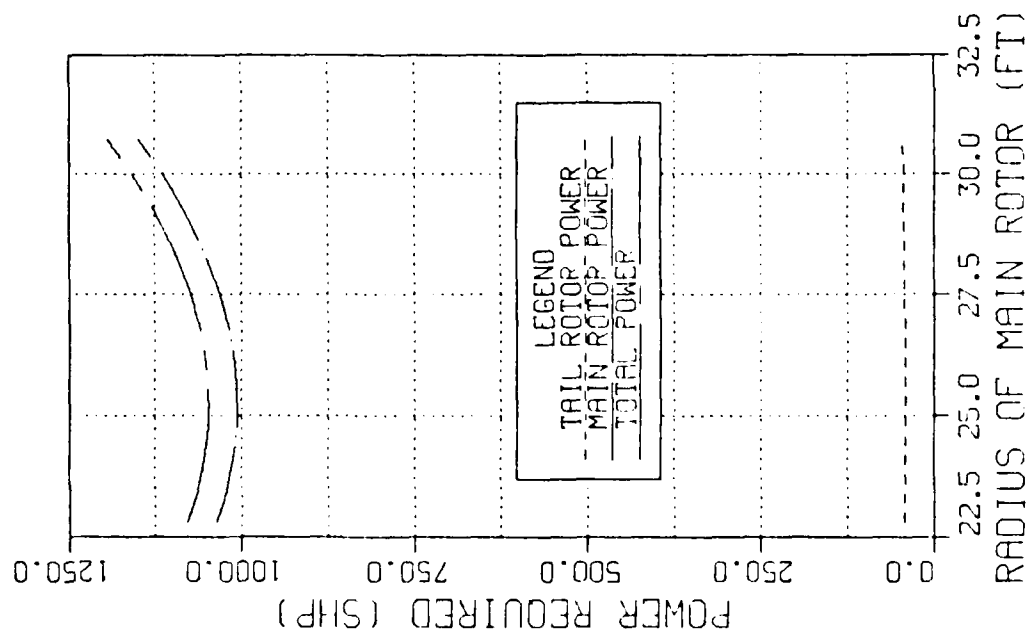
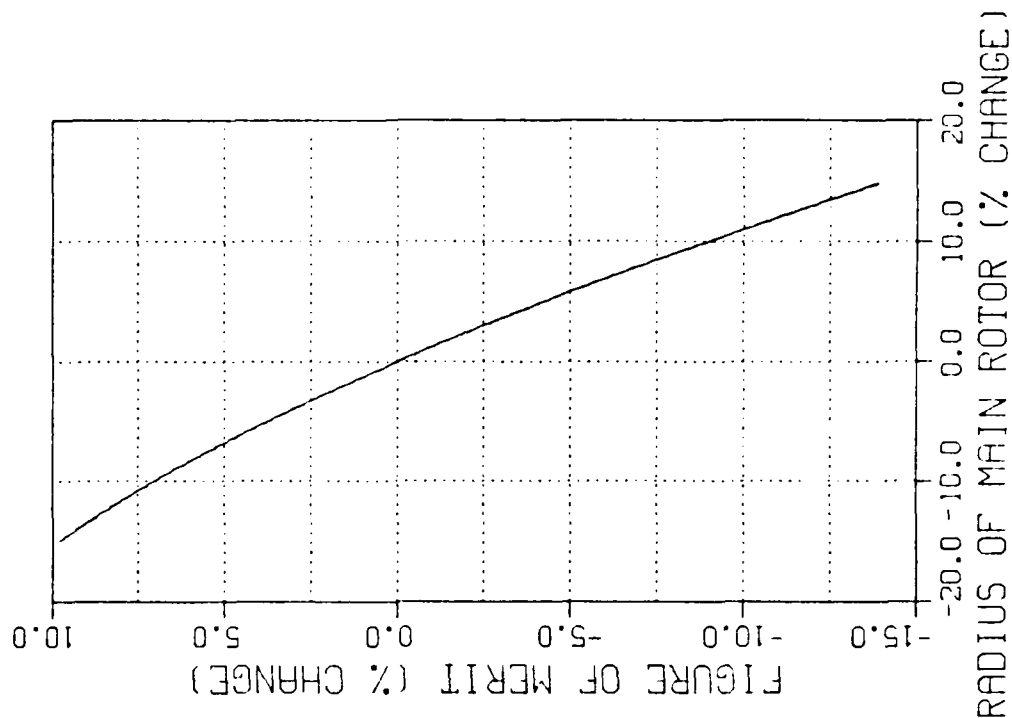
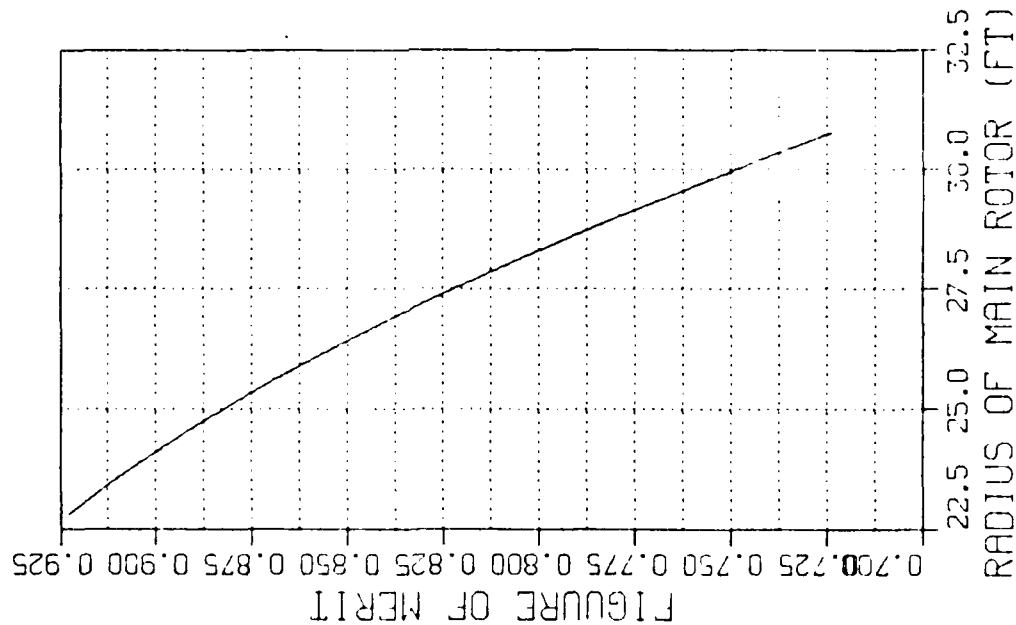
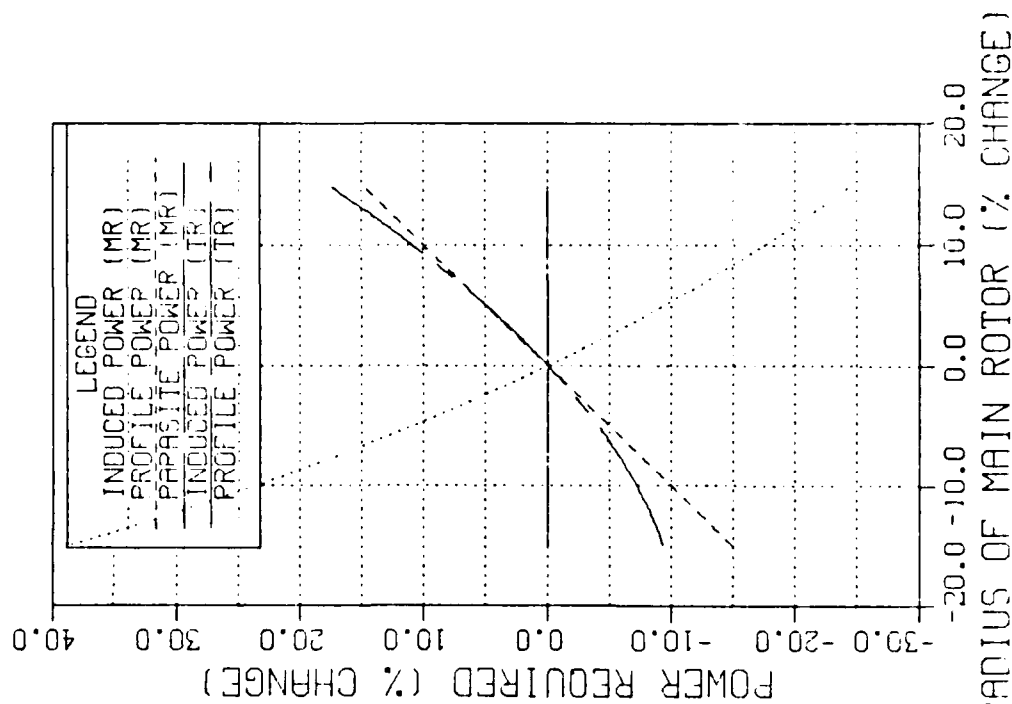
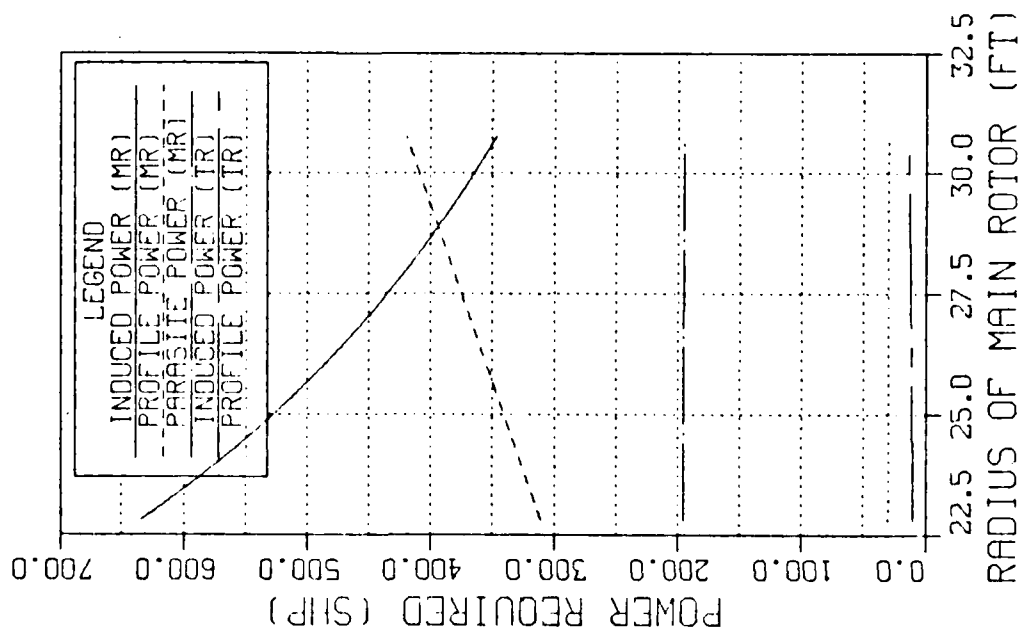


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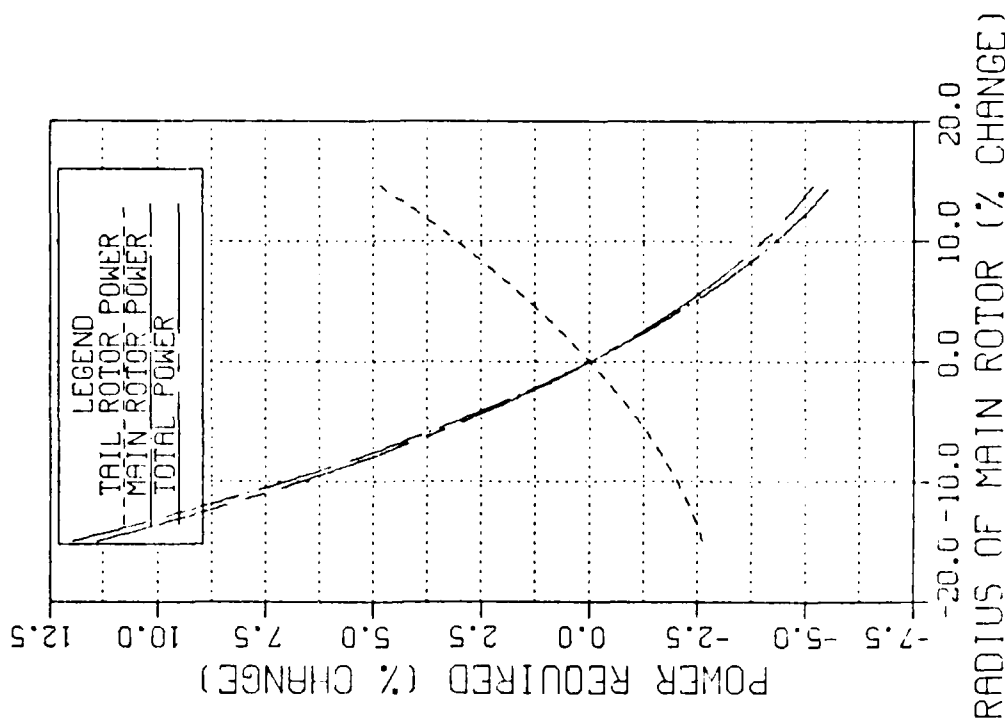
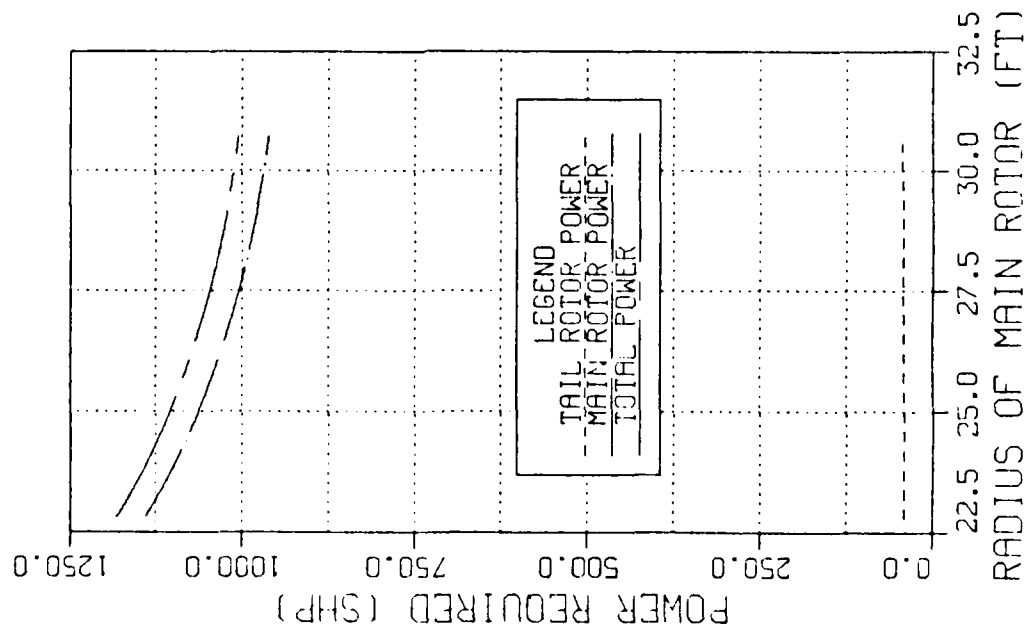
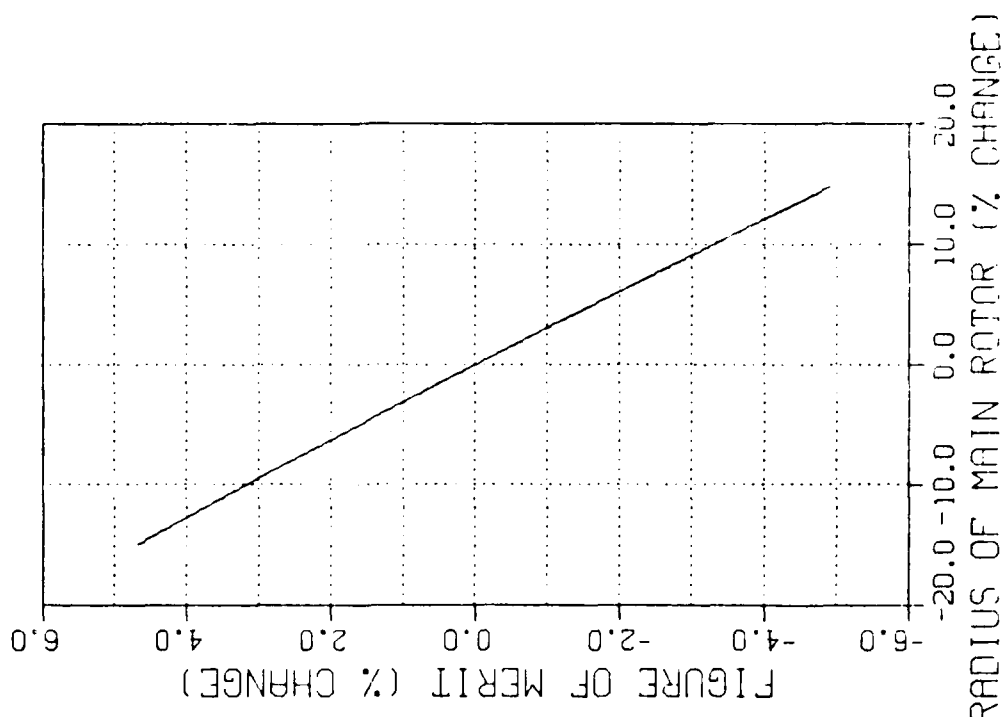
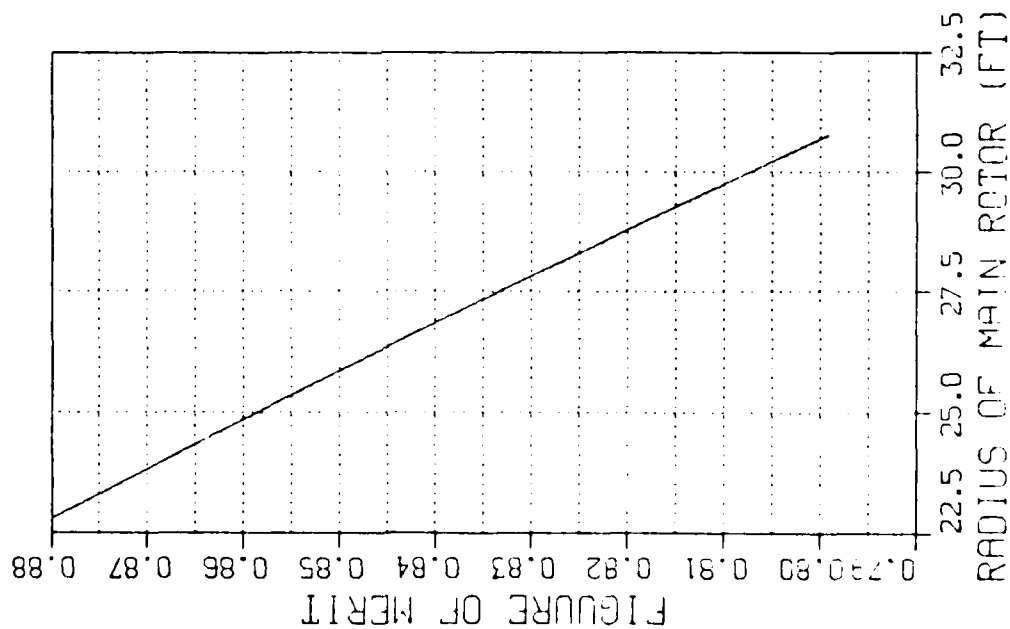


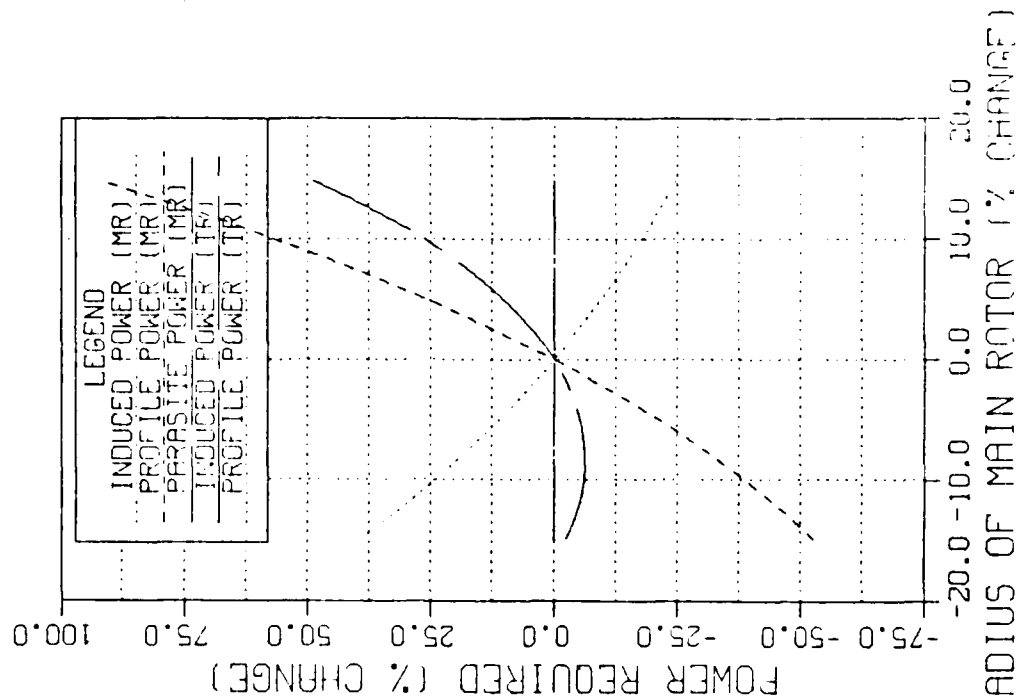
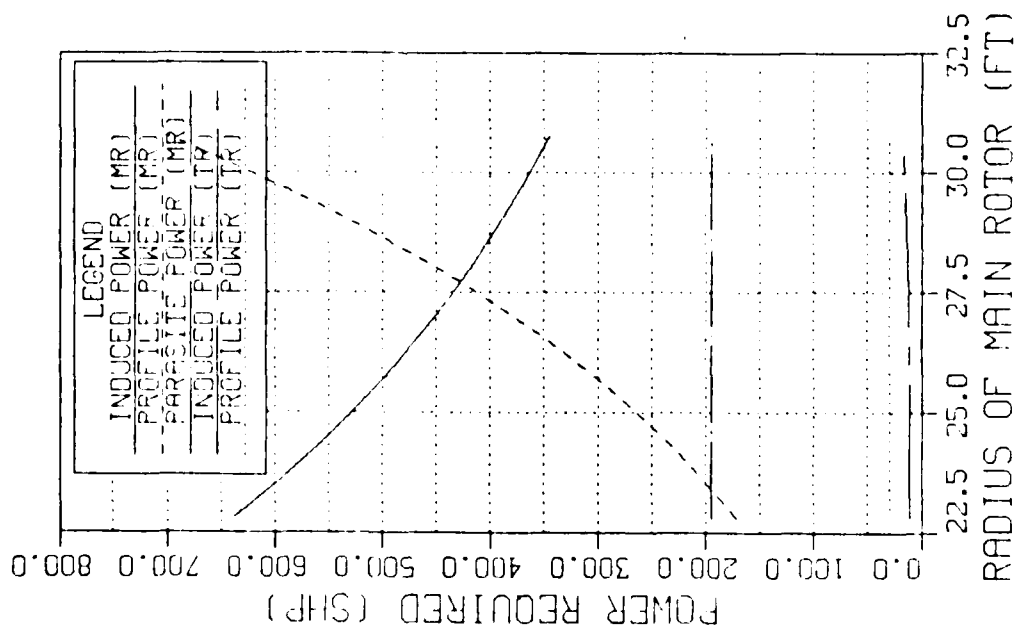


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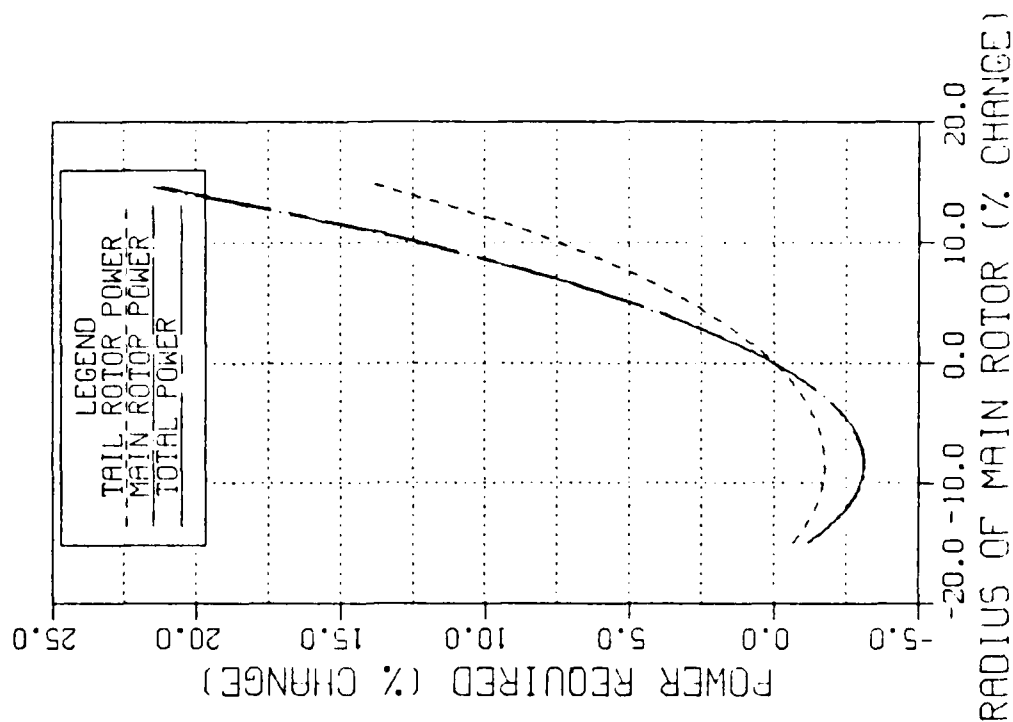
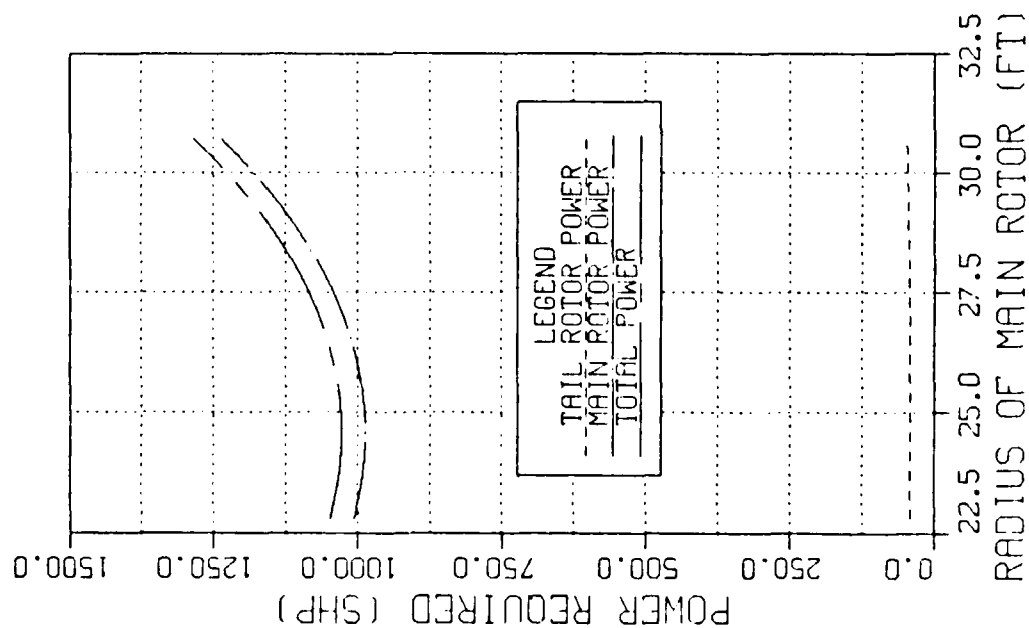
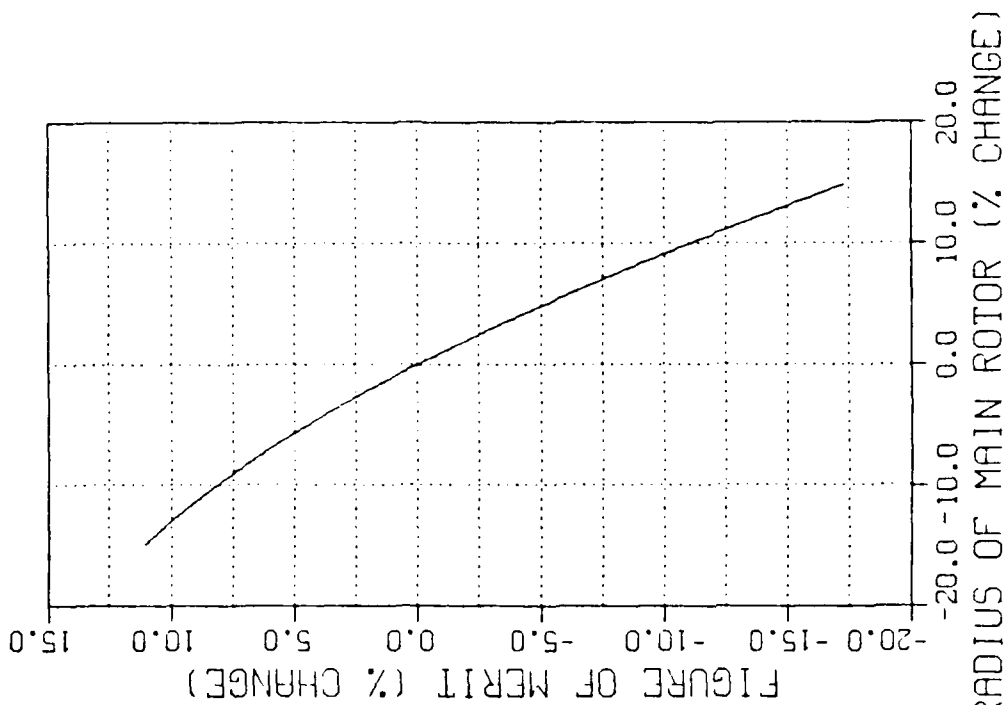
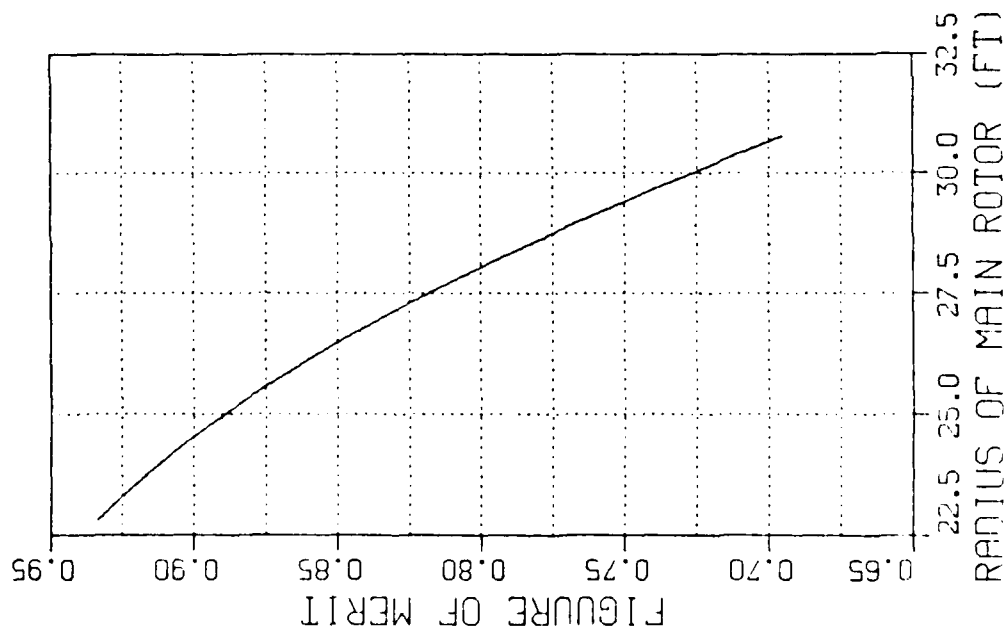
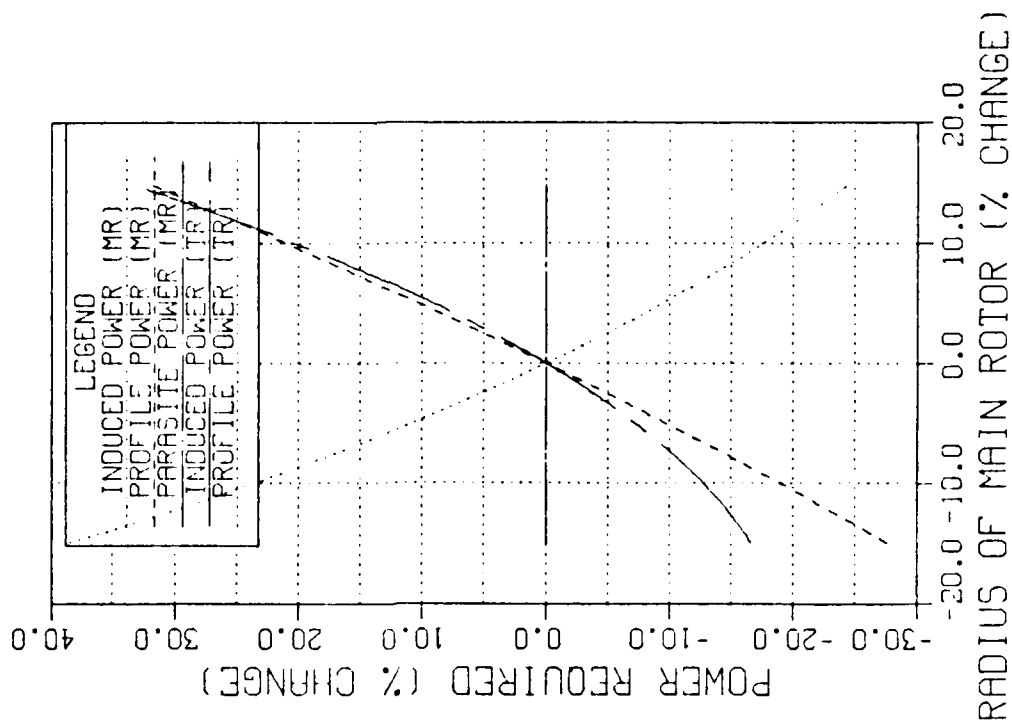
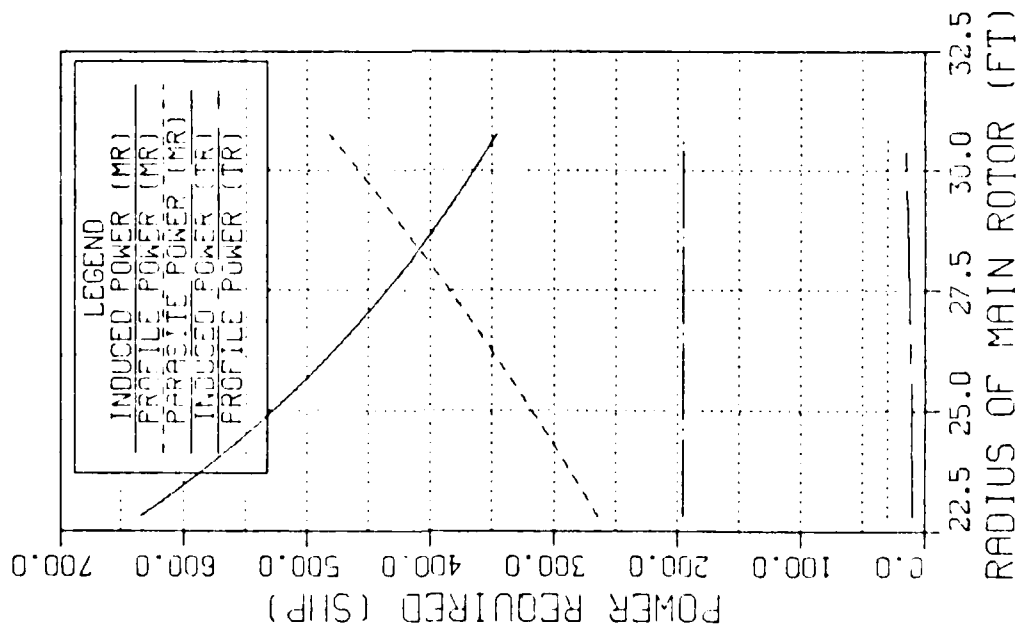


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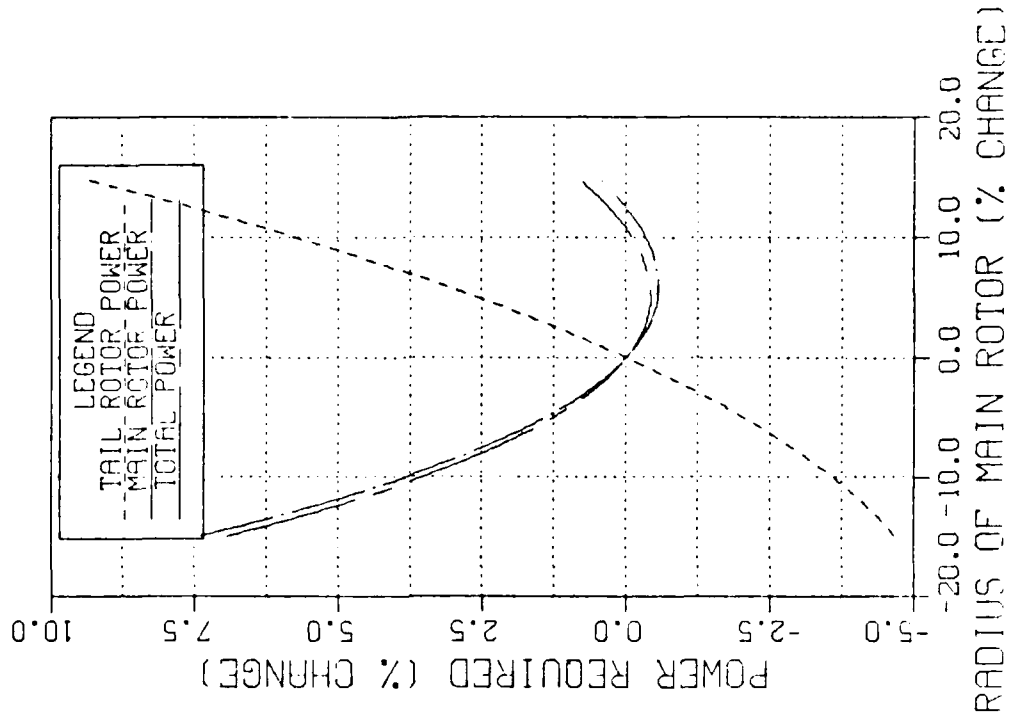
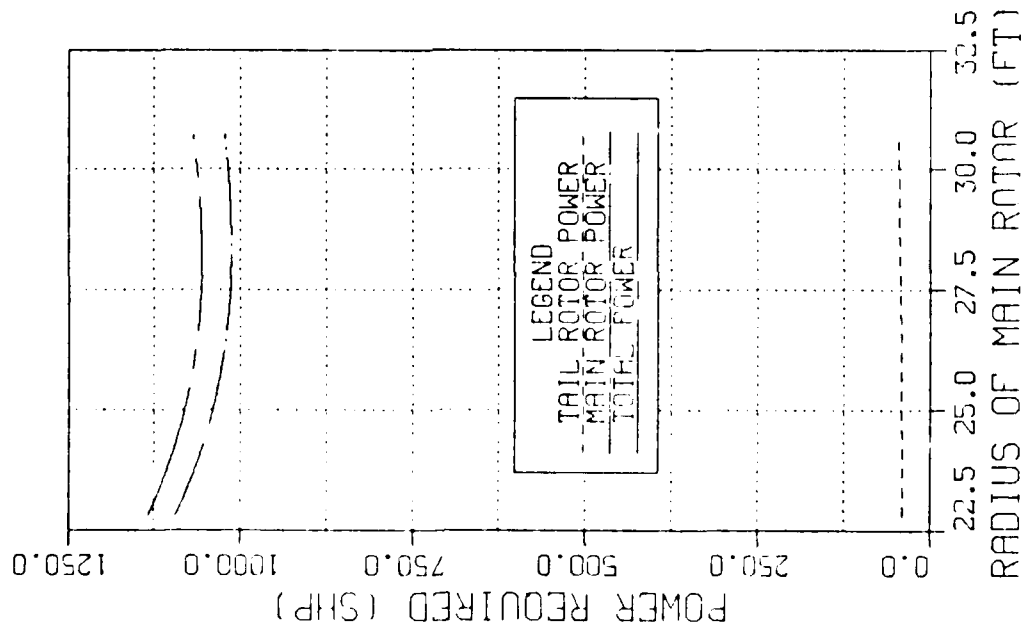
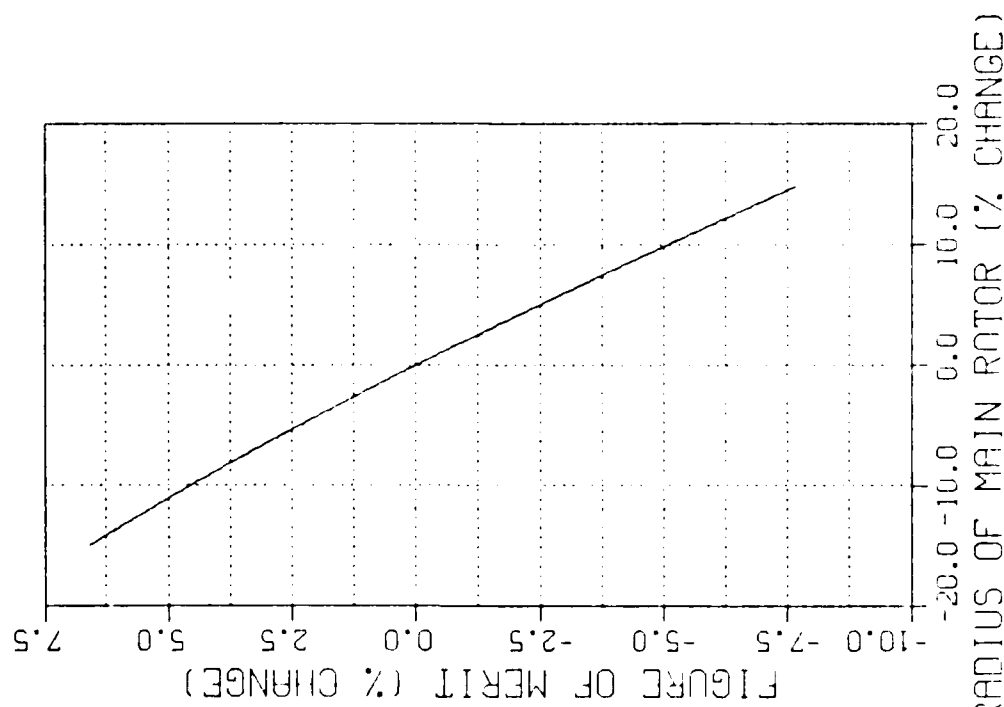
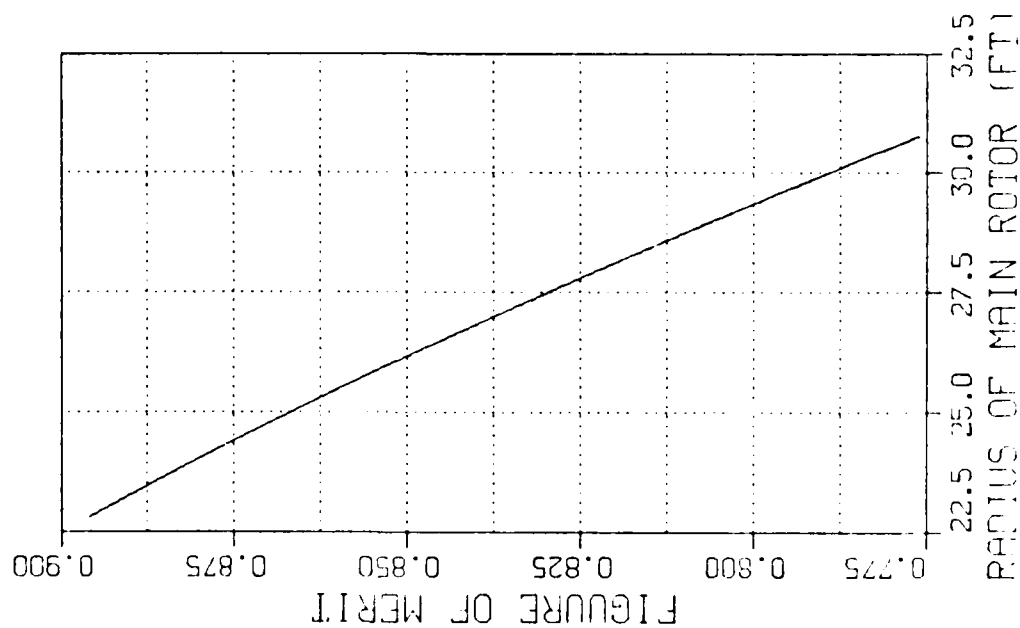


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 CHORD & ROTATIONAL VELOCITY  
 ALLOWED TO VARY WITH RADIUS

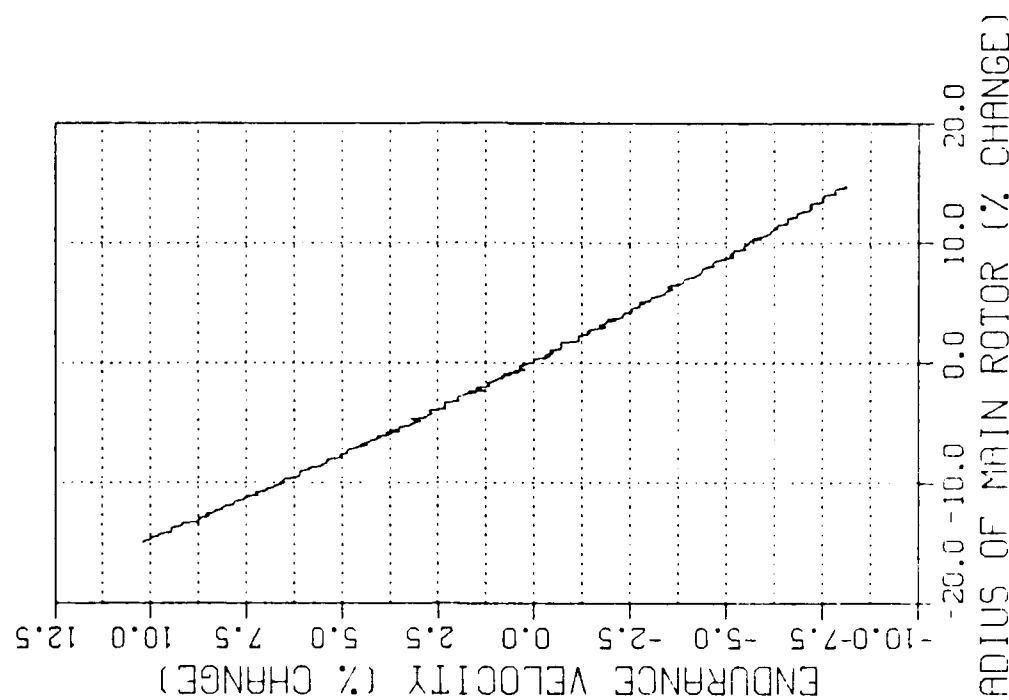
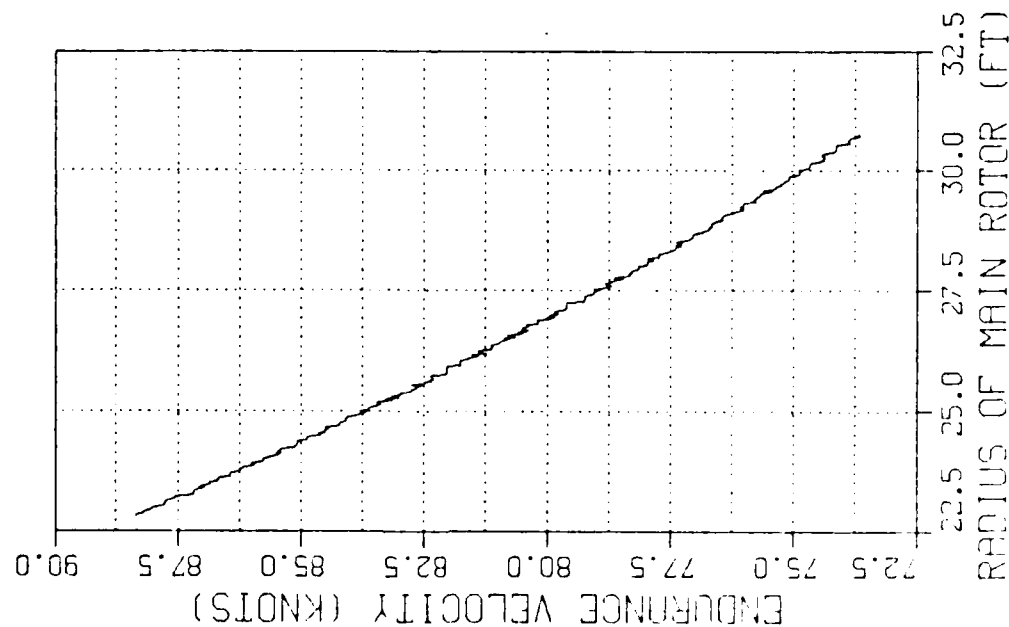


# ENDURANCE VELOCITY VERSUS RADIUS

CHORD & ROTATIONAL VELOCITY HELD CONSTANT

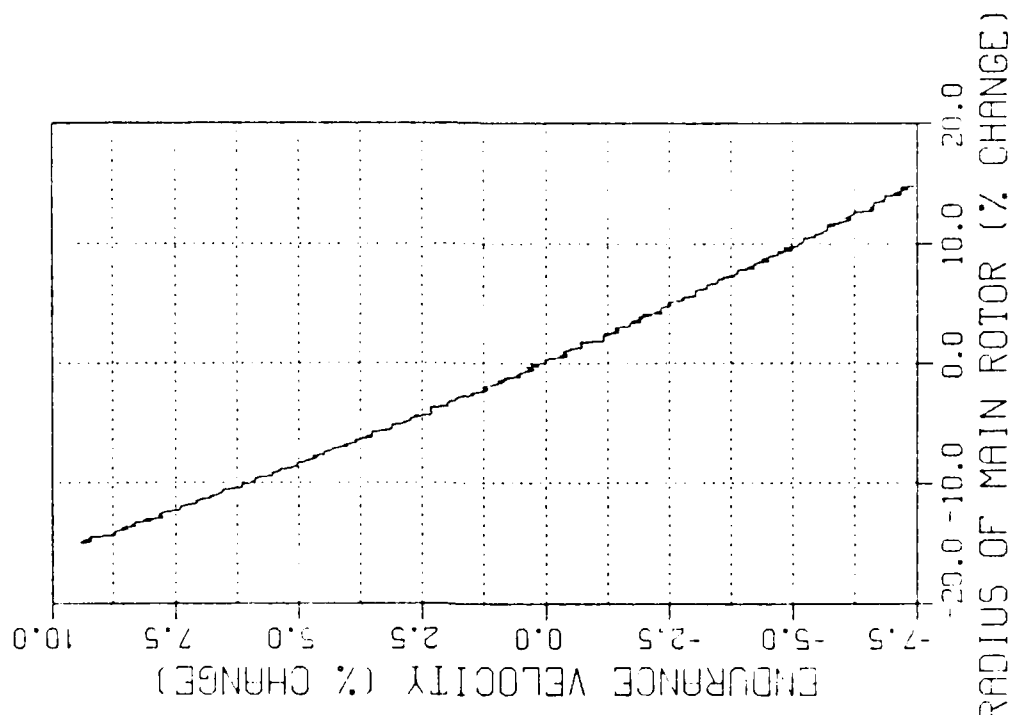
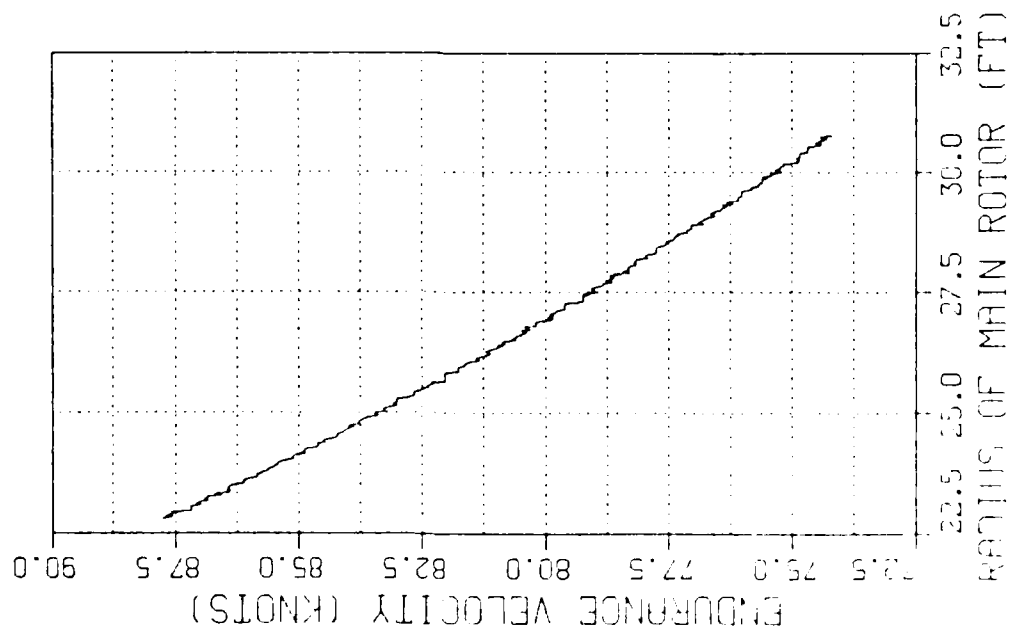
SOLIDITY, TIP VELOCITY & ADVANCE RATIO

ALLOWED TO VARY WITH RADIUS

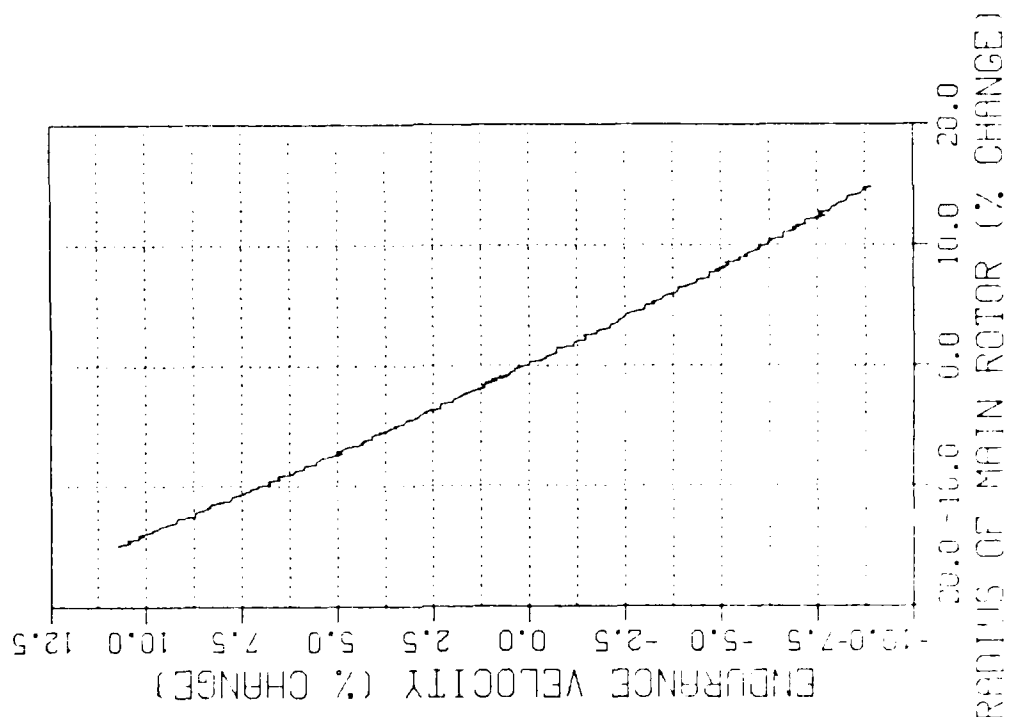
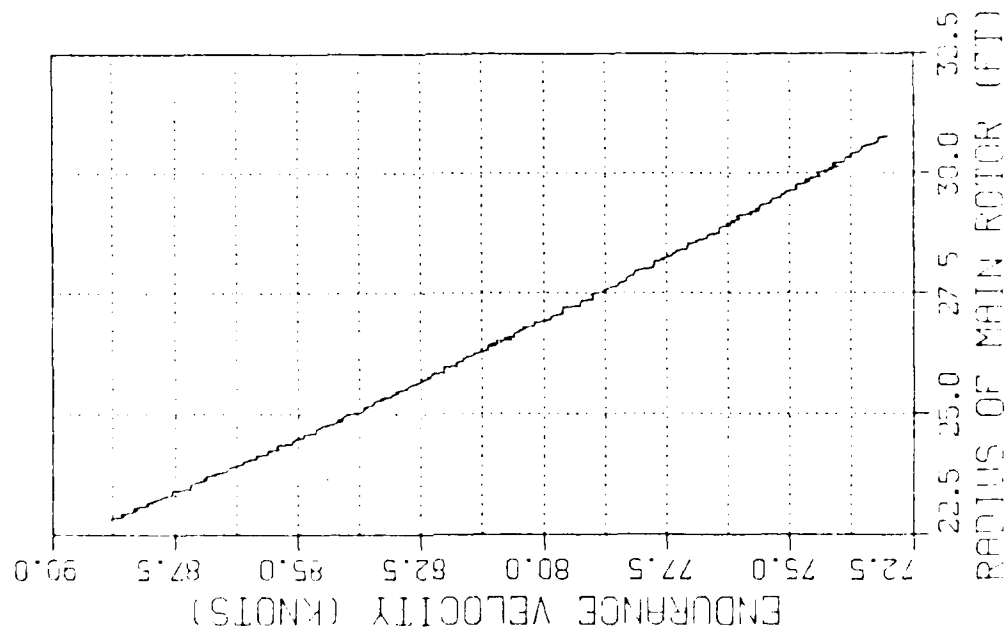




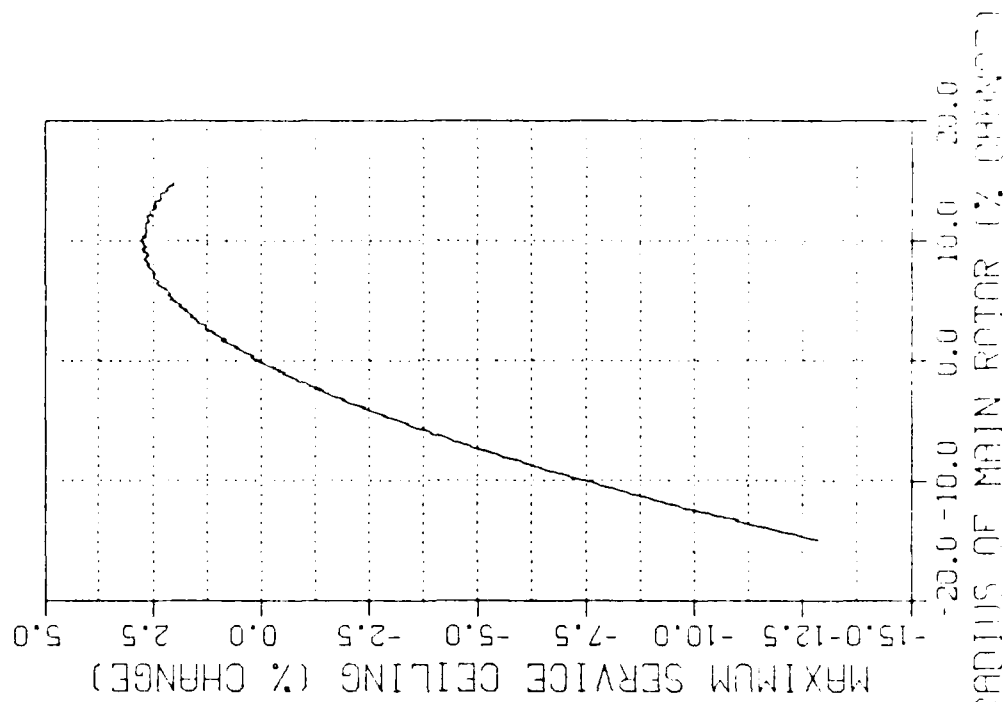
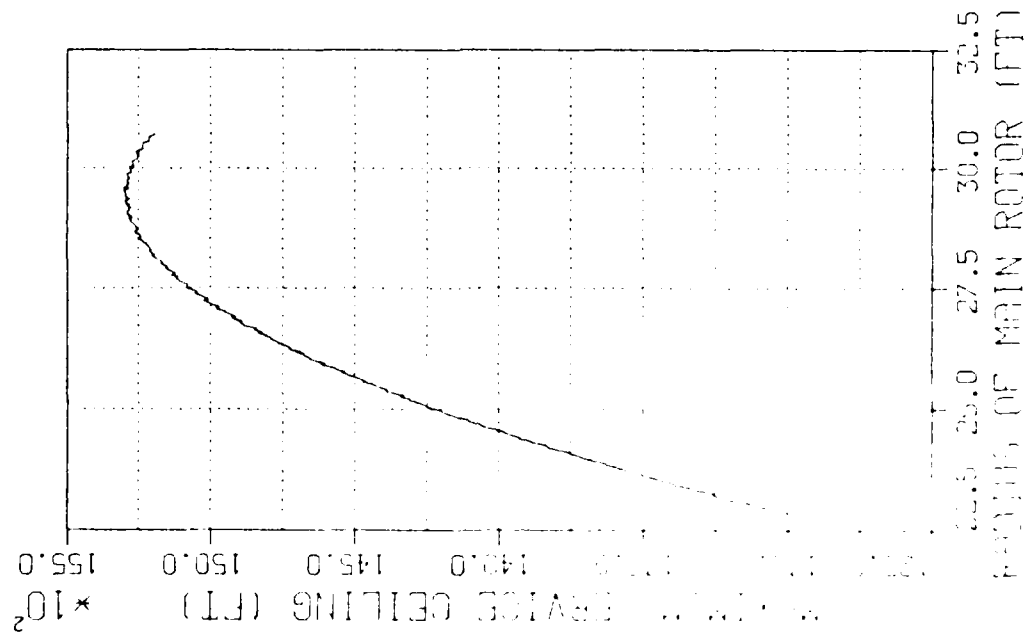
# ENDURANCE VELOCITY VERSUS RADIUS CHORD, TIP VELOCITY & ADVANCE RATIO HELD CONSTANT SOLIDITY, ROTATIONAL VELOCITY ALLOWED TO VARY WITH RADIUS



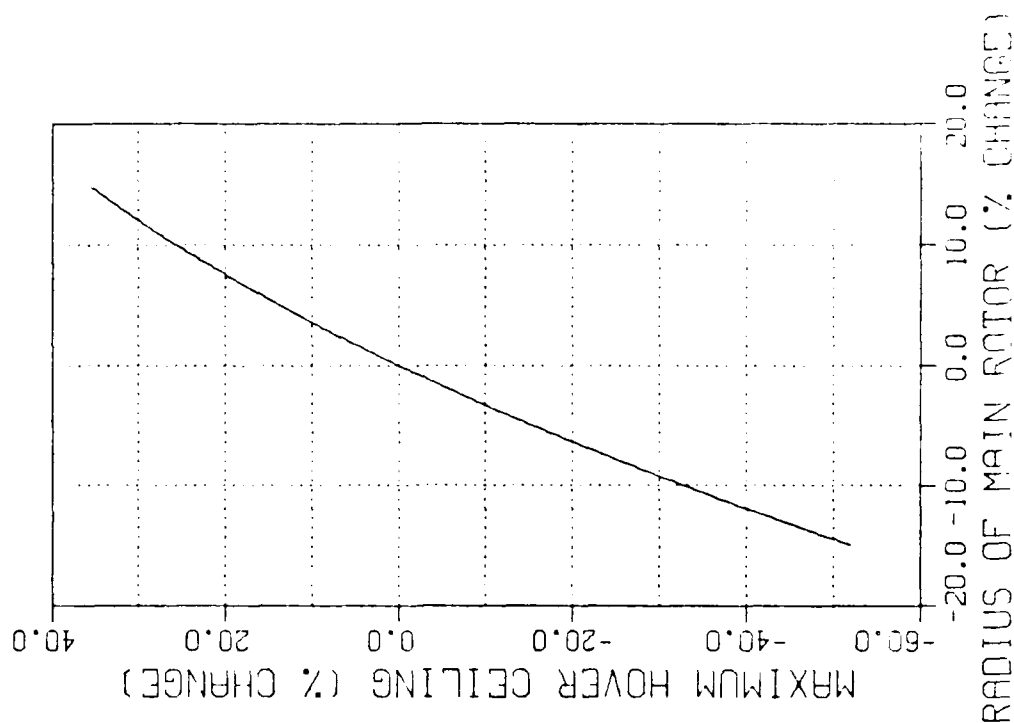
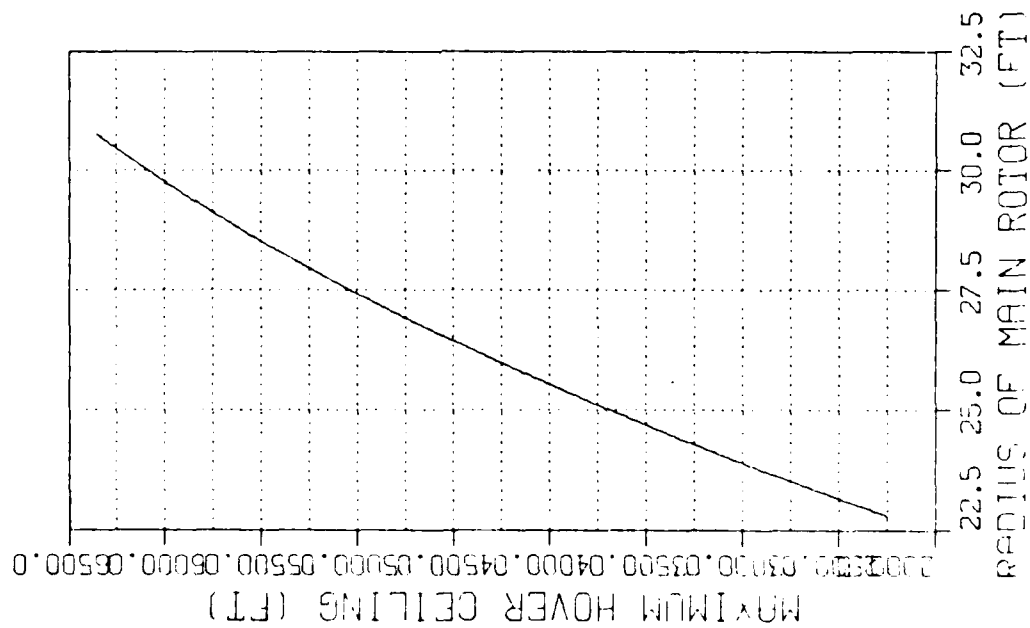
# ENDURANCE VELOCITY VERSUS RADIUS SOLIDITY & ROTATIONAL VELOCITY HELD CONSTANT CHORD, ADVANCE RATIO & TIP VELOCITY ALLOWED TO VARY WITH RADIUS



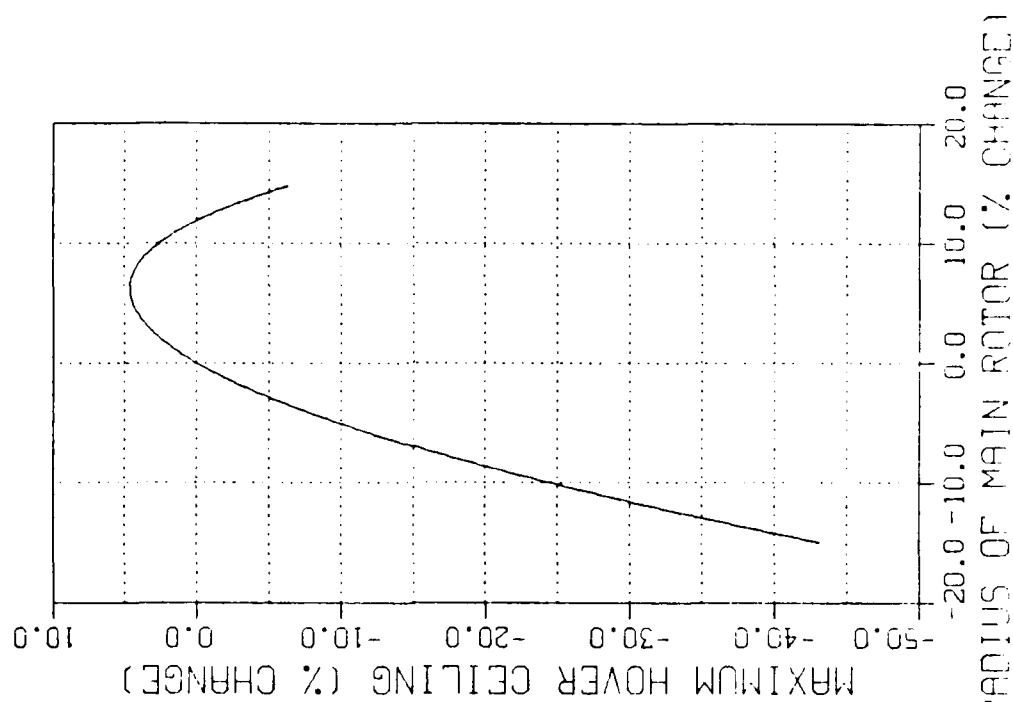
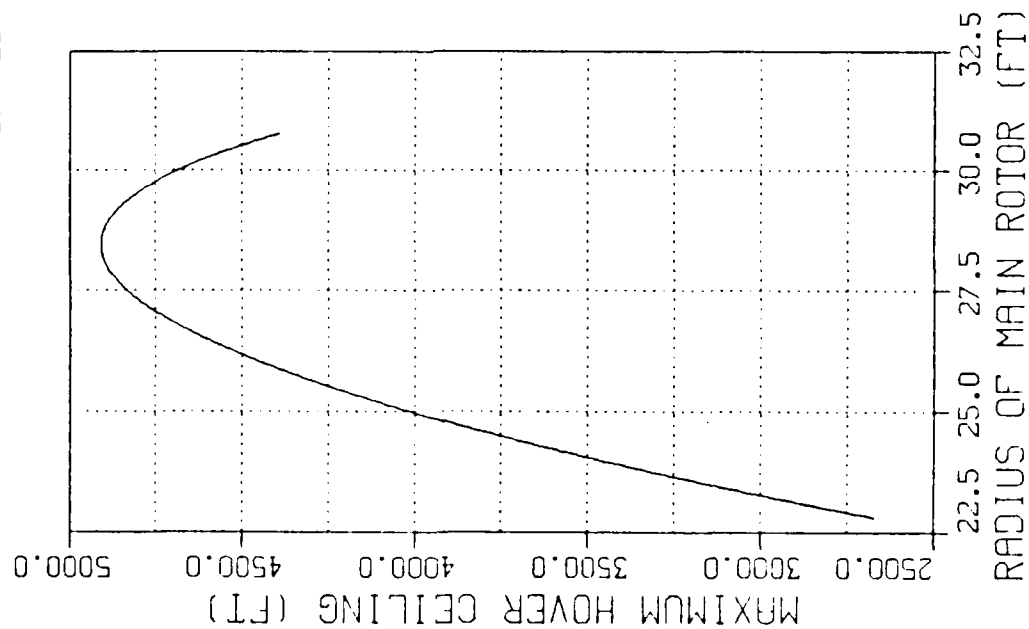
# MAXIMUM SERVICE CEILING VERSUS RADIUS CHANGE CHORD & ROTATIONAL VELOCITY HELD CONSTANT SOLIDITY, TIP VELOCITY & ADVANCE RATIO ALLOWED TO VARY WITH RADIUS



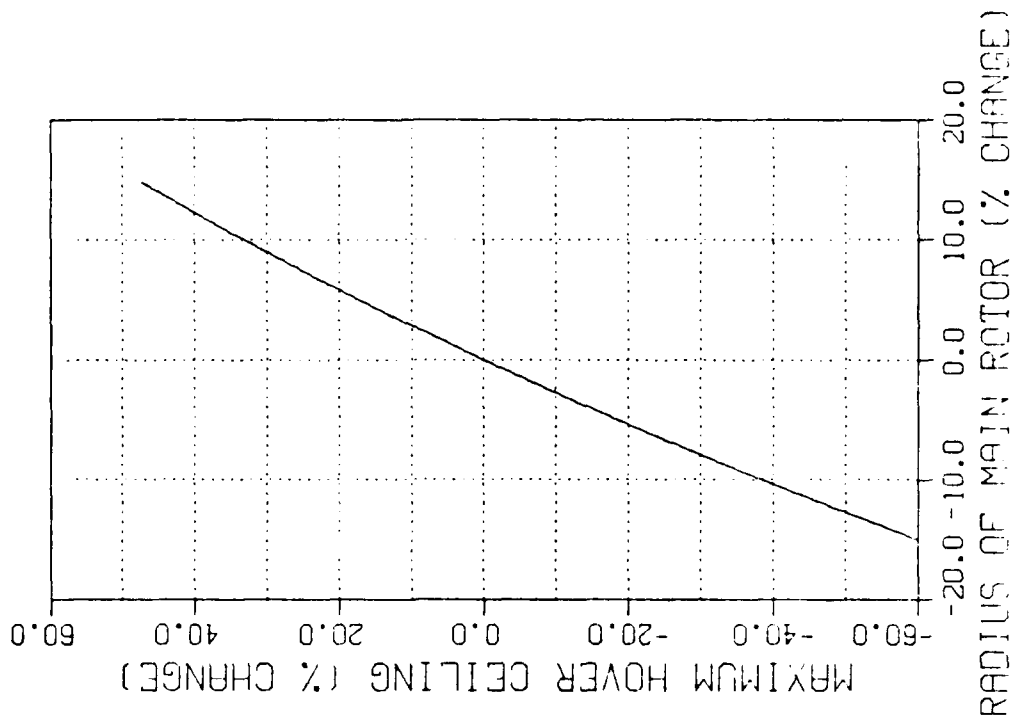
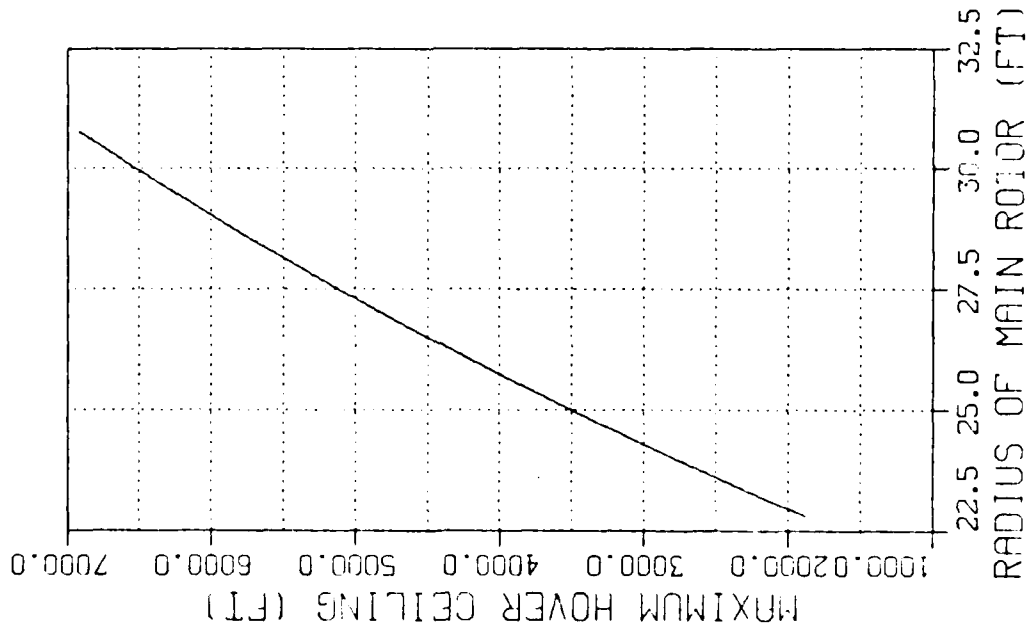
MAXIMUM HOVER CEILING (IGE) VERSUS RADIUS  
 SOLIDITY, ADVANCE RATIO & TIP VELOCITY HELD CONSTANT  
 CHORD & ROTATIONAL VELOCITY  
 ALLOWED TO VARY WITH RADIUS



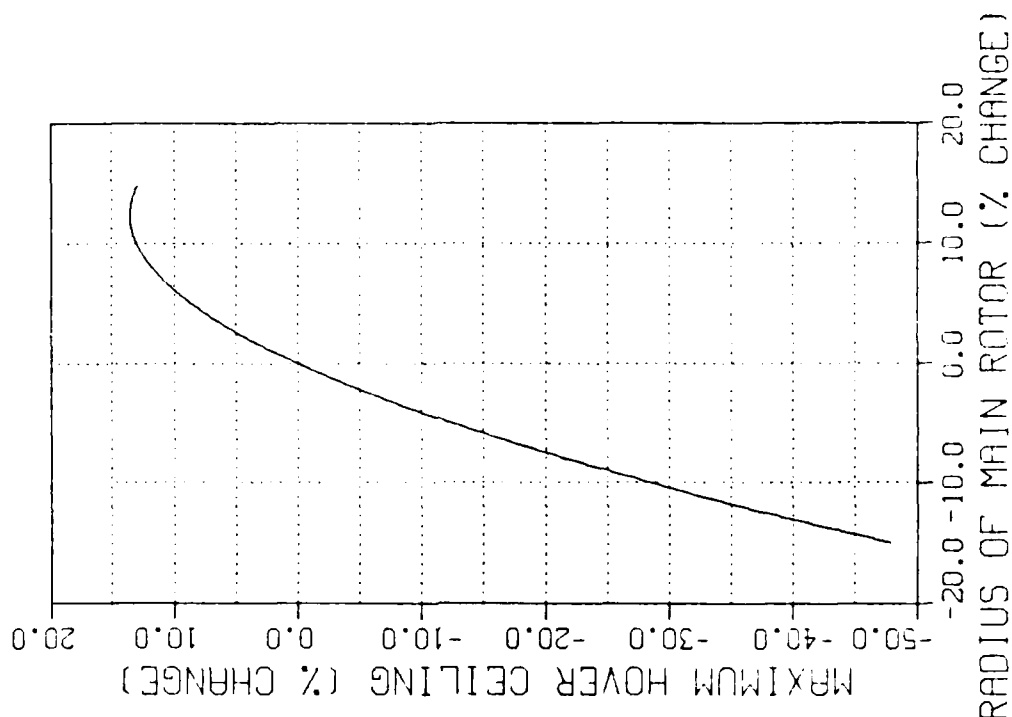
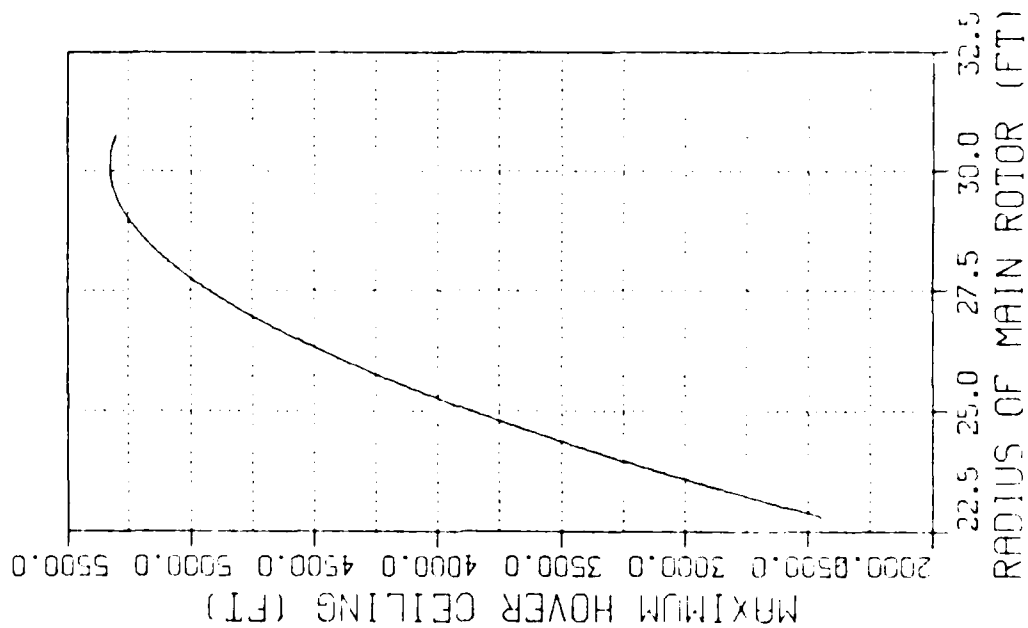
MAXIMUM HOVER CEILING (IGE) VERSUS RADIUS  
 SOLIDITY & ROTATIONAL VELOCITY HELD CONSTANT  
 CHORD, ADVANCE RATIO & TIP VELOCITY  
 ALLOWED TO VARY WITH RADIUS



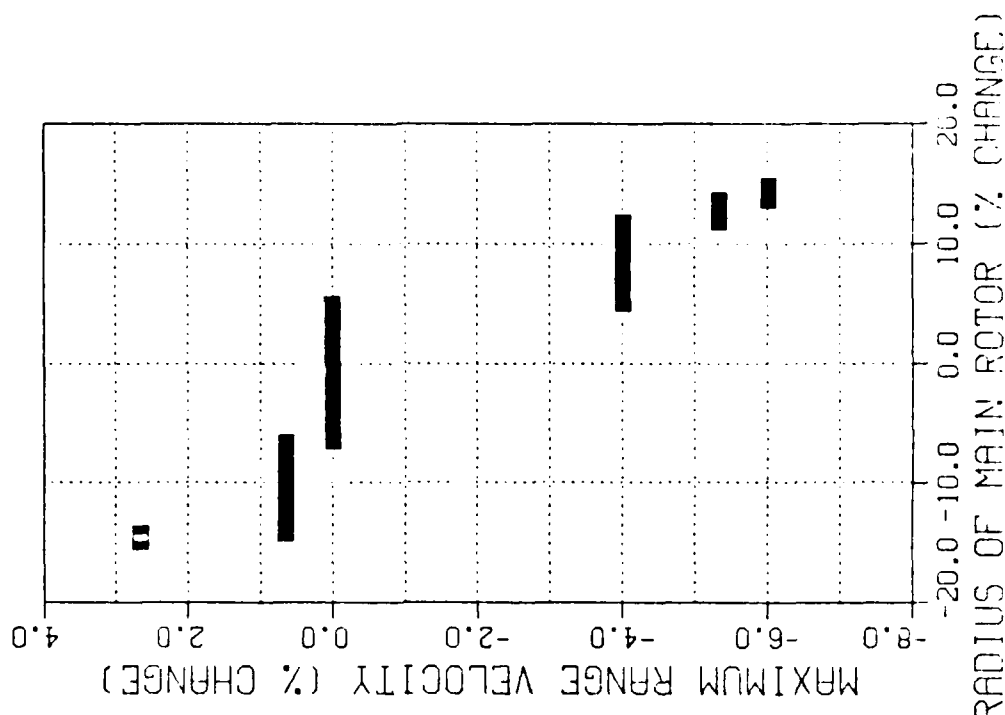
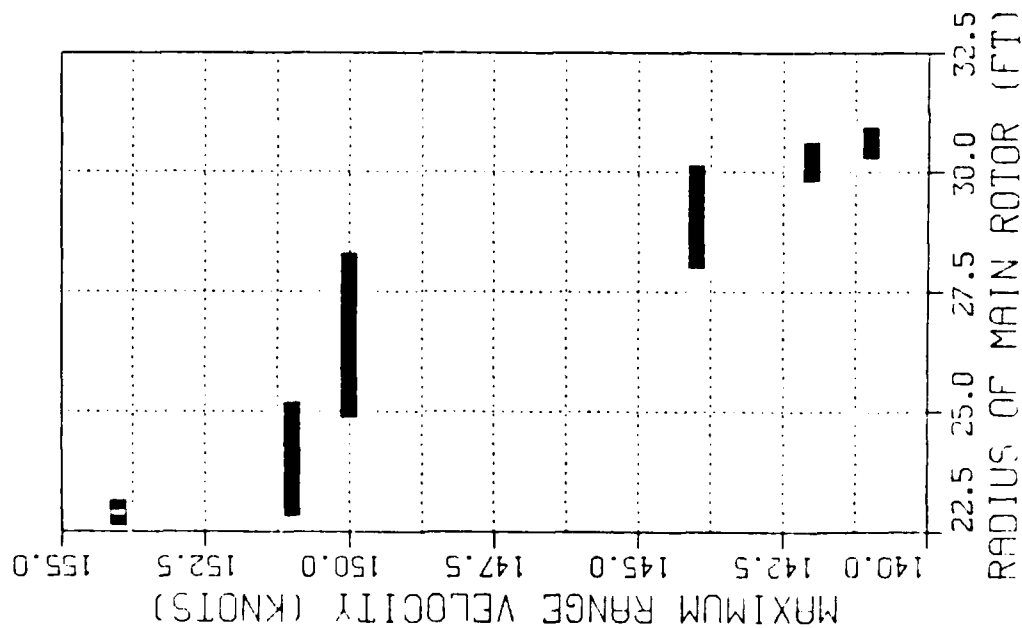
MAXIMUM HOVER CEILING (IGE) VERSUS RADIUS  
 CHORD, TIP VELOCITY & ADVANCE RATIO HELD CONSTANT  
 SOLIDITY, ROTATIONAL VELOCITY  
 ALLOWED TO VARY WITH RADIUS



MAXIMUM HOVER CEILING (IGE) VERSUS RADIUS  
 CHORD & ROTATIONAL VELOCITY HELD CONSTANT  
 SOLIDITY, TIP VELOCITY & ADVANCE RATIO  
 ALLOWED TO VARY WITH RADIUS

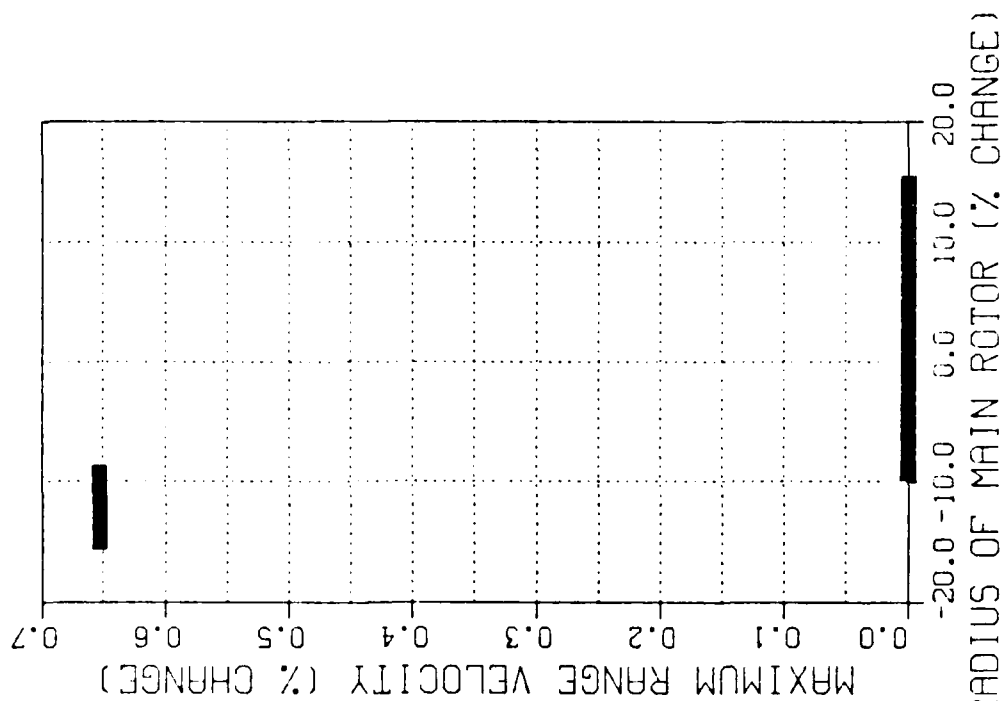
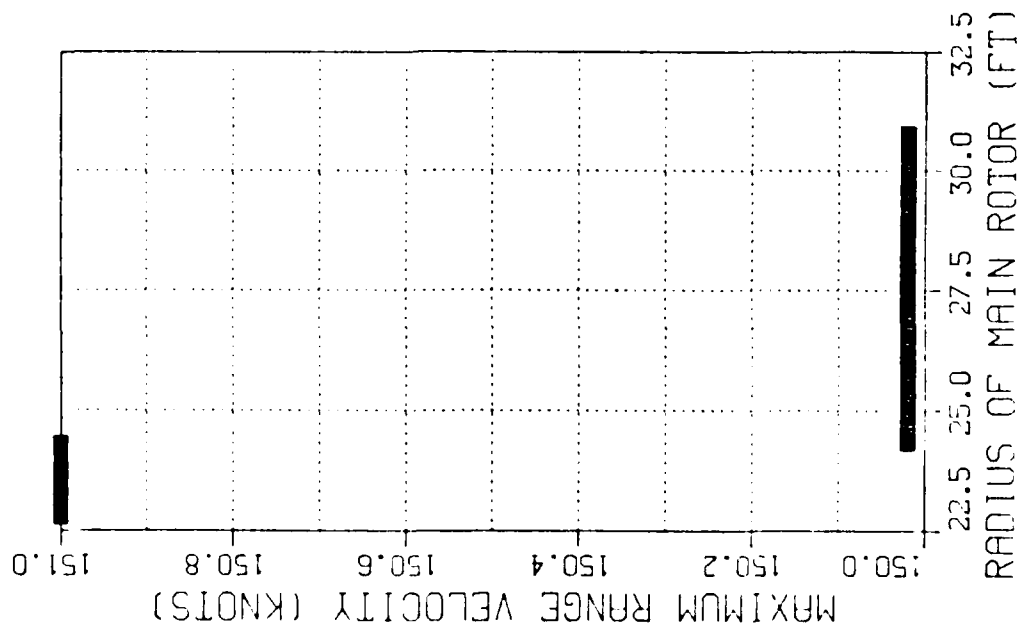


# MAXIMUM RANGE VELOCITY VERSUS RADIUS CHANGE SOLIDITY, ADVANCE RATIO & TIP VELOCITY HELD CONSTANT CHORD & ROTATIONAL VELOCITY ALLOWED TO VARY WITH RADIUS

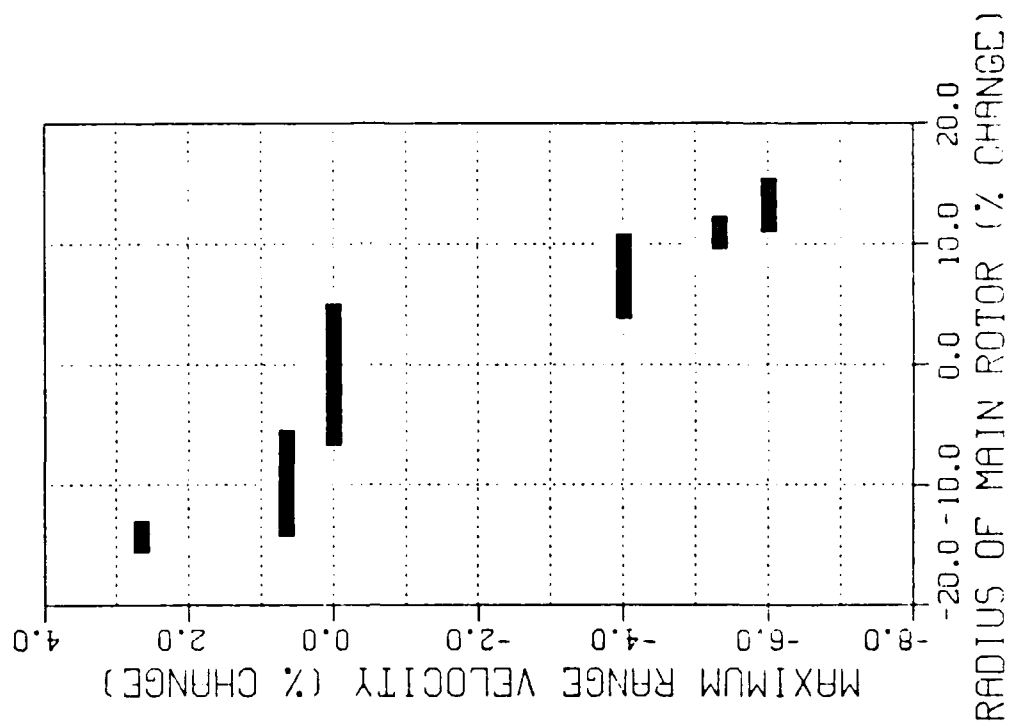
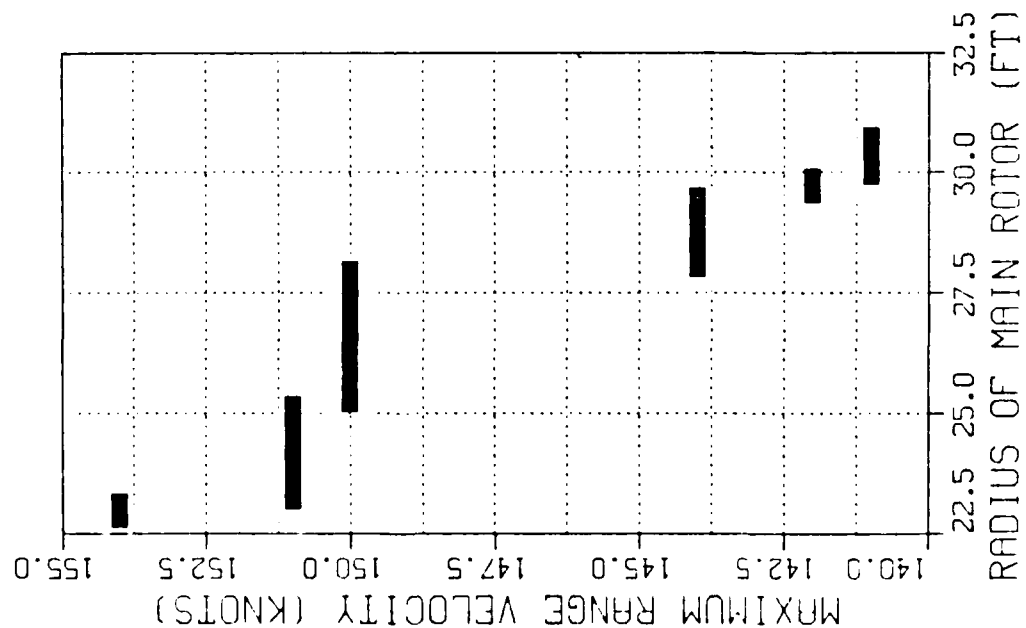




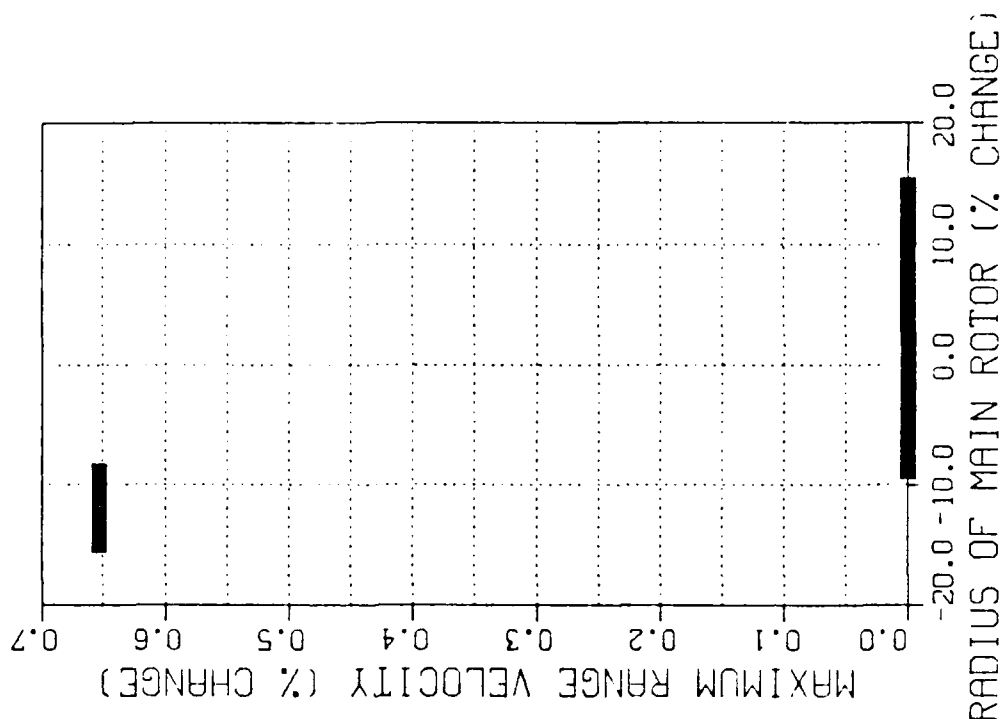
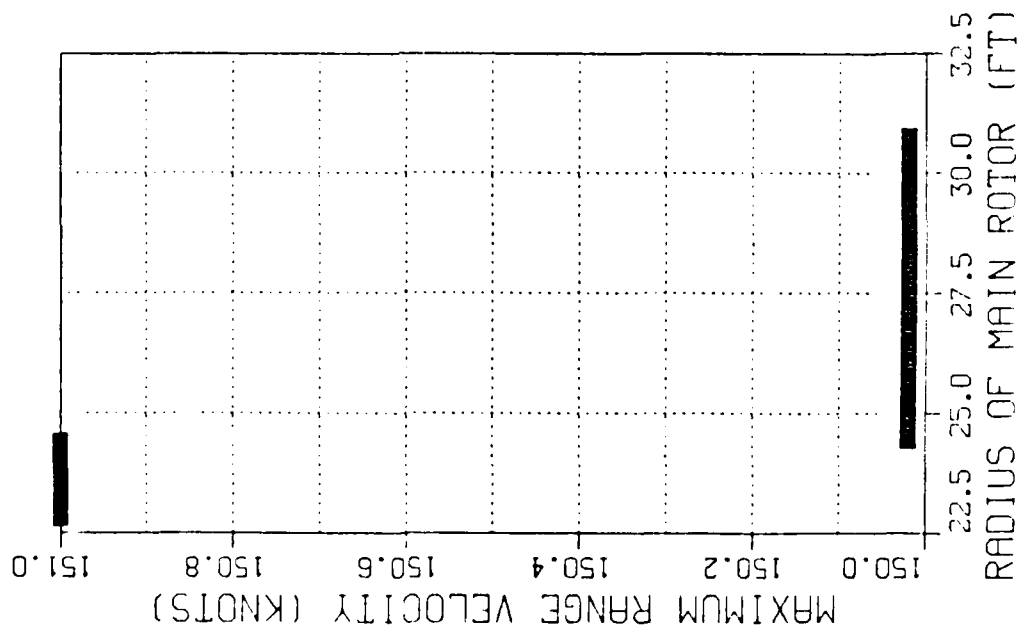
# MAXIMUM RANGE VELOCITY VERSUS RADIUS CHANGE SOLIDITY & ROTATIONAL VELOCITY HELD CONSTANT CHORD, ADVANCE RATIO & TIP VELOCITY ALLOWED TO VARY WITH RADIUS



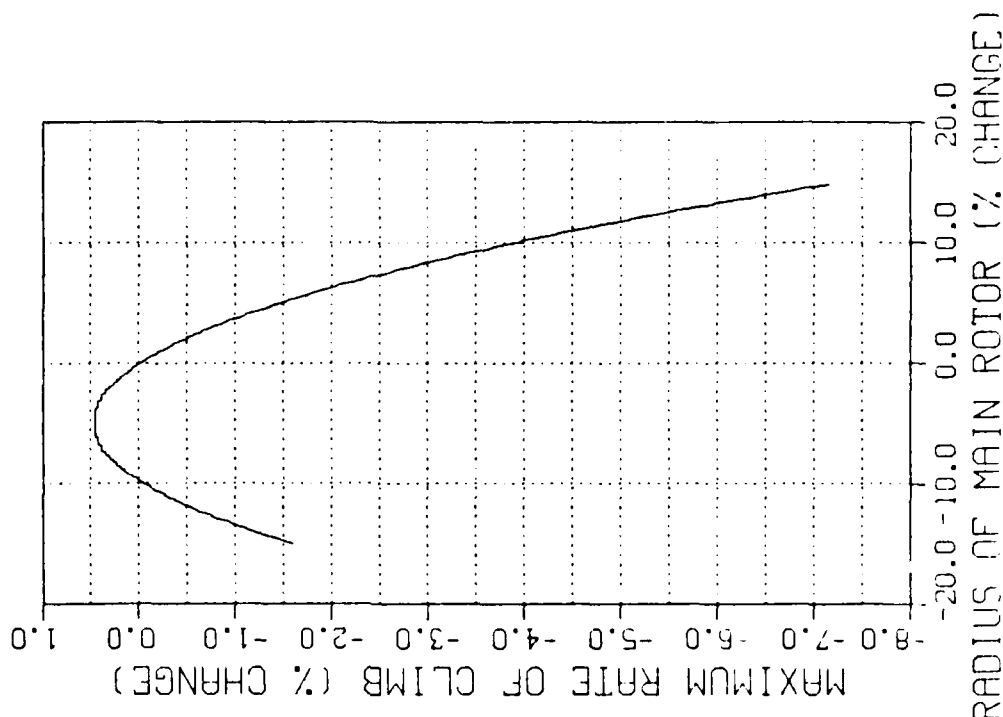
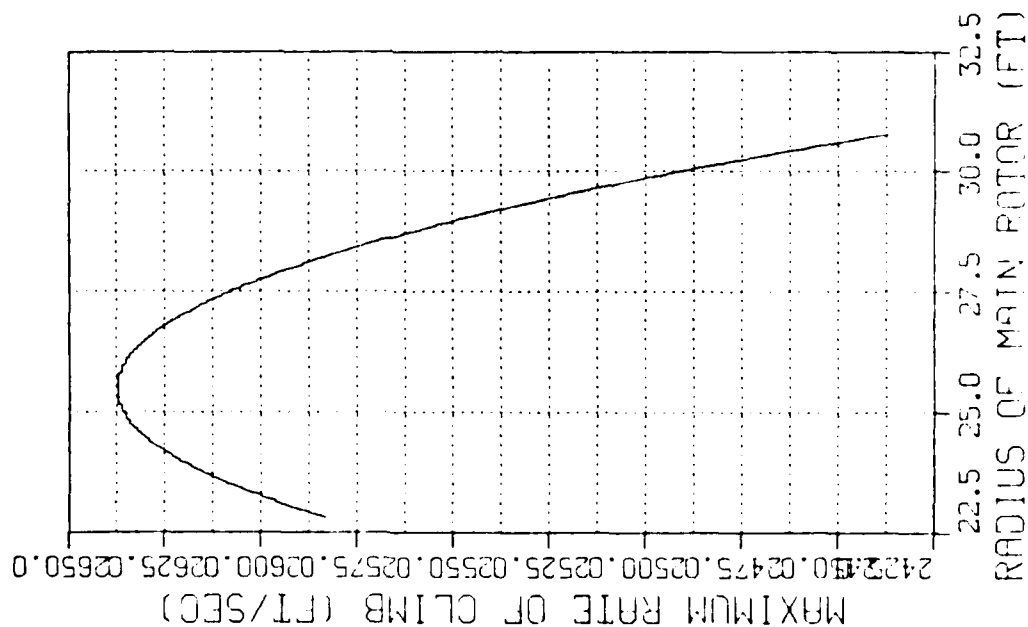
# MAXIMUM RANGE VELOCITY VERSUS RADIUS CHANGE CHORD, TIP VELOCITY & ADVANCE RATIO HELD CONSTANT SOLIDITY, ROTATIONAL VELOCITY ALLOWED TO VARY WITH RADIUS



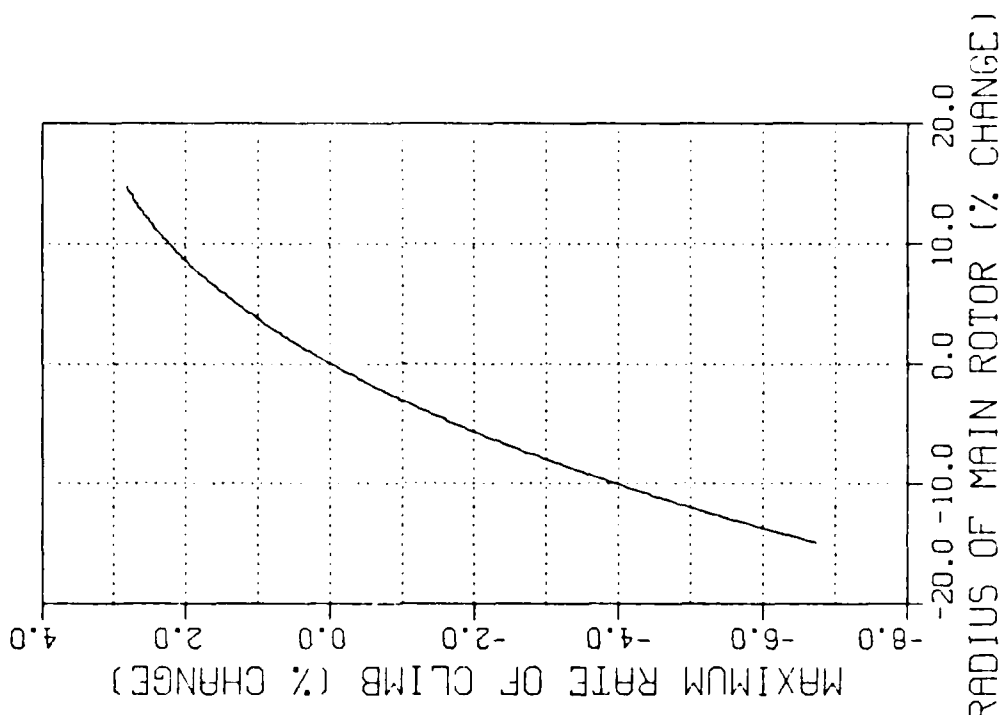
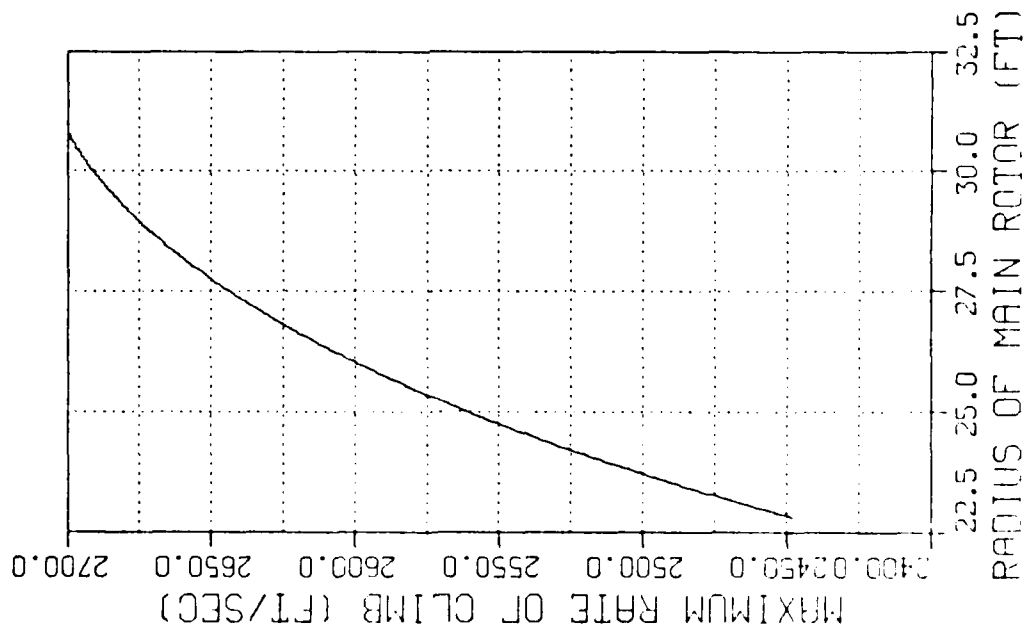
# MAXIMUM RANGE VELOCITY VERSUS RADIUS CHANGE CHORD & ROTATIONAL VELOCITY HELD CONSTANT SOLIDITY, TIP VELOCITY & ADVANCE RATIO ALLOWED TO VARY WITH RADIUS



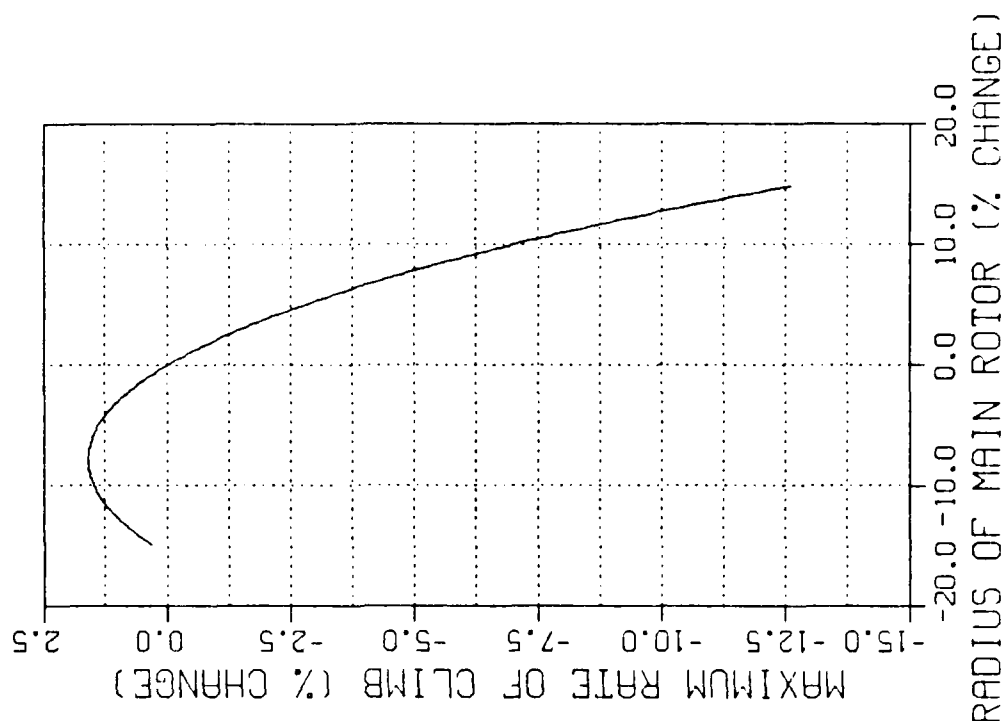
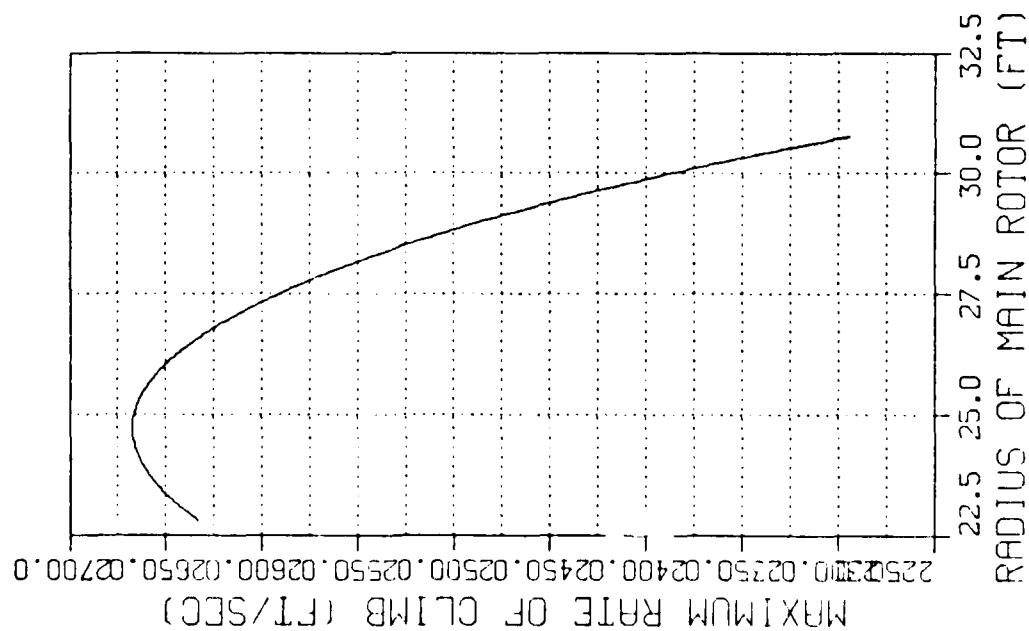
# MAXIMUM RATE OF CLIMB VERSUS RADIUS CHANGE CHORD & ROTATIONAL VELOCITY HELD CONSTANT SOLIDITY, TIP VELOCITY & ADVANCE RATIO ALLOWED TO VARY WITH RADIUS



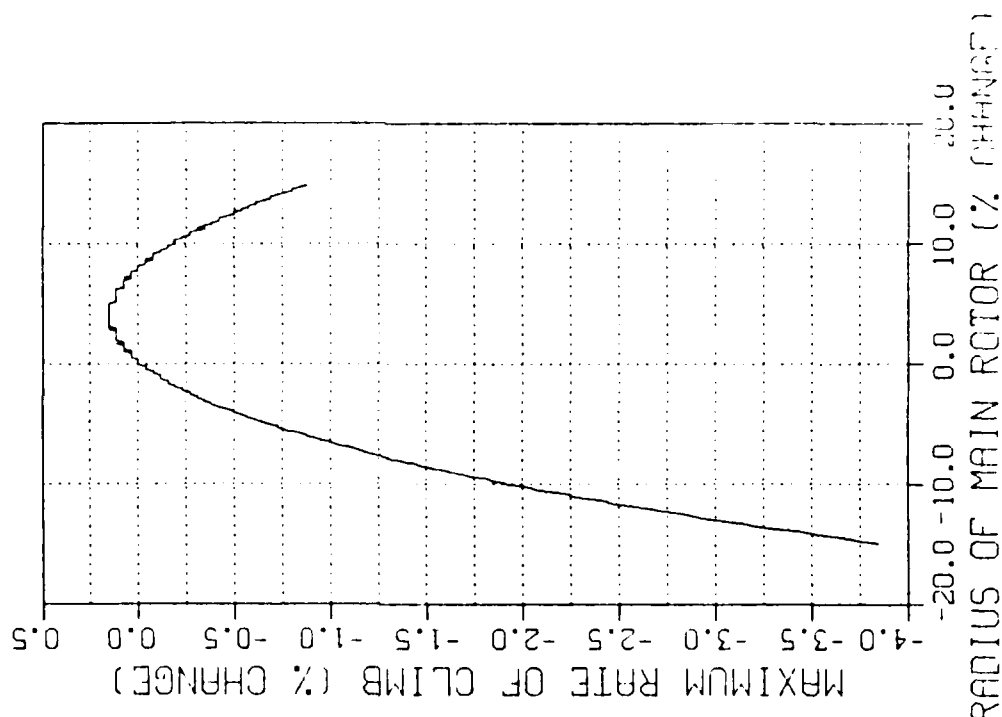
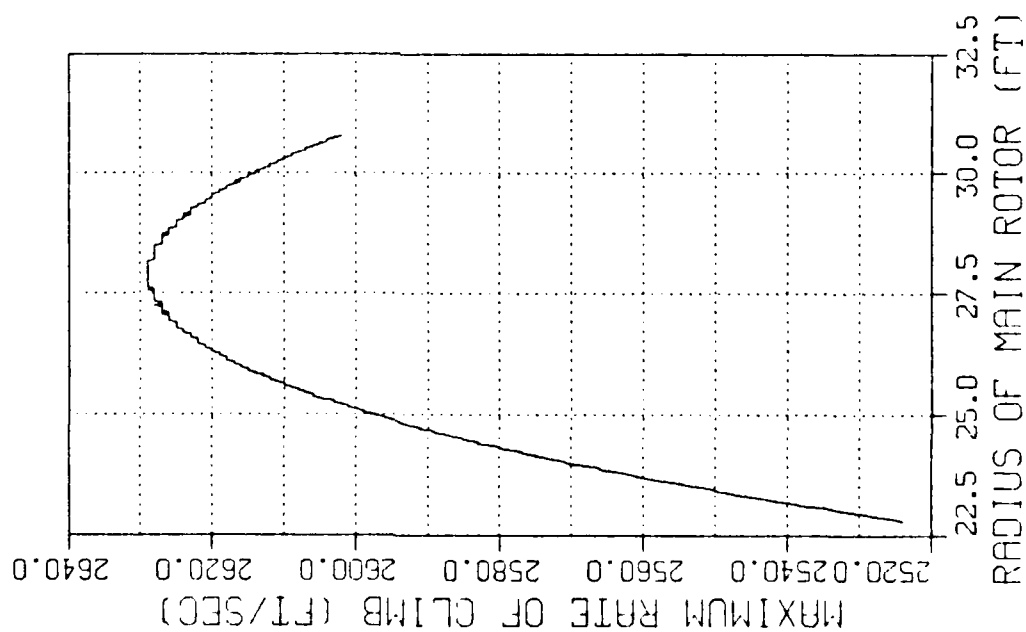
# MAXIMUM RATE OF CLIMB VERSUS RADIUS CHANGE CHORD, TIP VELOCITY & ADVANCE RATIO HELD CONSTANT SOLIDITY, ROTATIONAL VELOCITY ALLOWED TO VARY WITH RADIUS



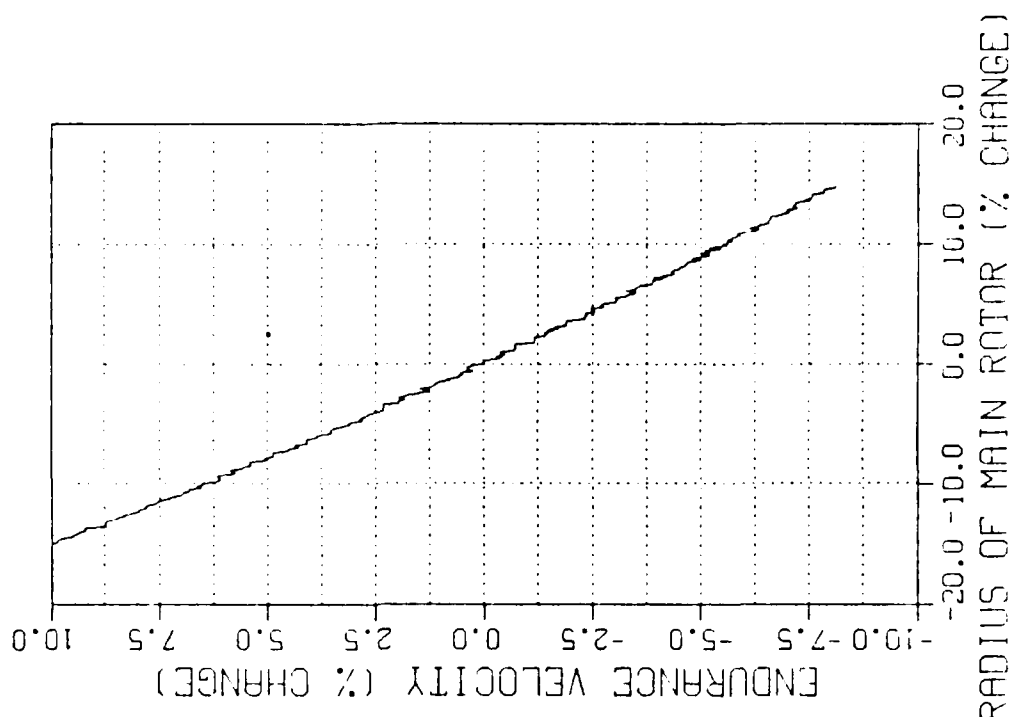
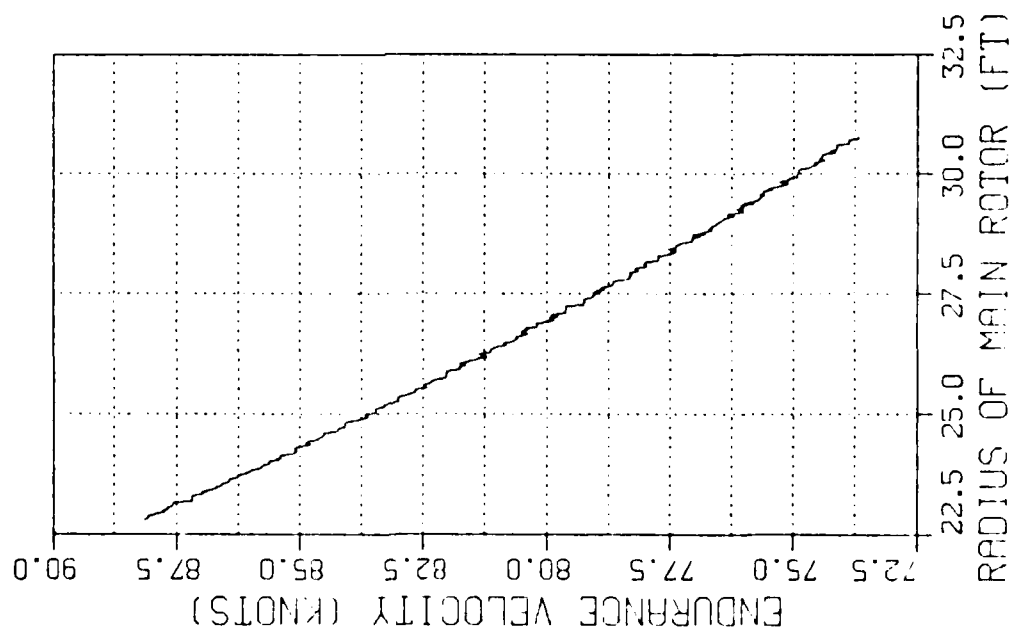
MAXIMUM RATE OF CLIMB VERSUS RADIUS CHANGE  
 SOLIDITY & ROTATIONAL VELOCITY HELD CONSTANT  
 CHORD, ADVANCE RATIO & TIP VELOCITY  
 ALLOWED TO VARY WITH RADIUS



# MAXIMUM RATE OF CLIMB VERSUS RADIUS CHANGE SOLIDITY, ADVANCE RATIO & TIP VELOCITY HELD CONSTANT CHORD & ROTATIONAL VELOCITY ALLOWED TO VARY WITH RADIUS

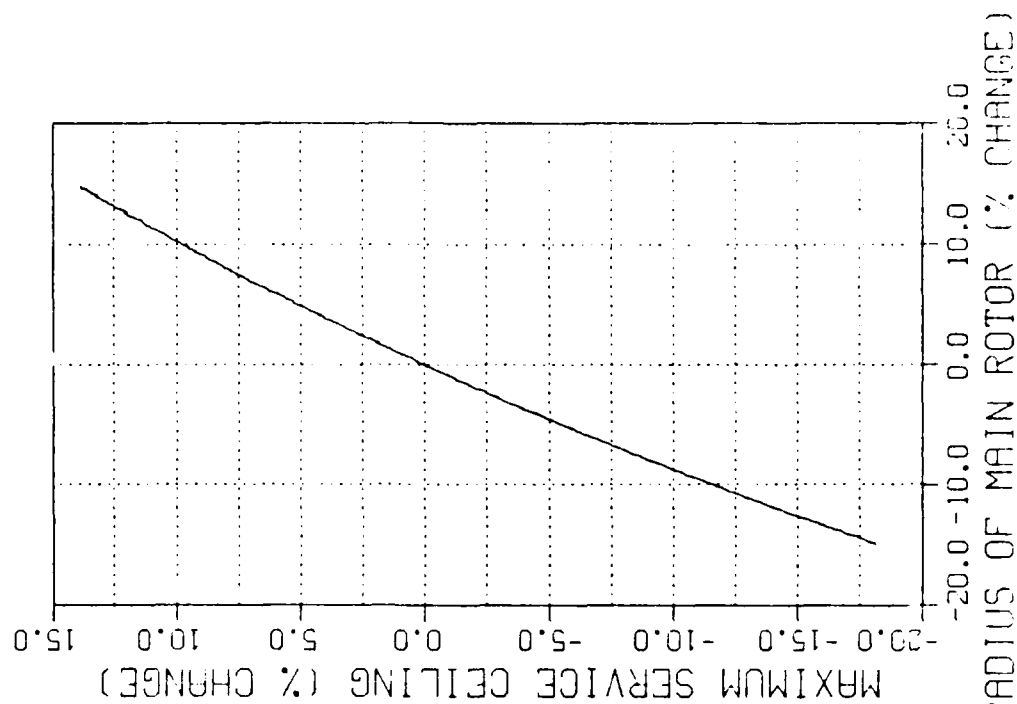
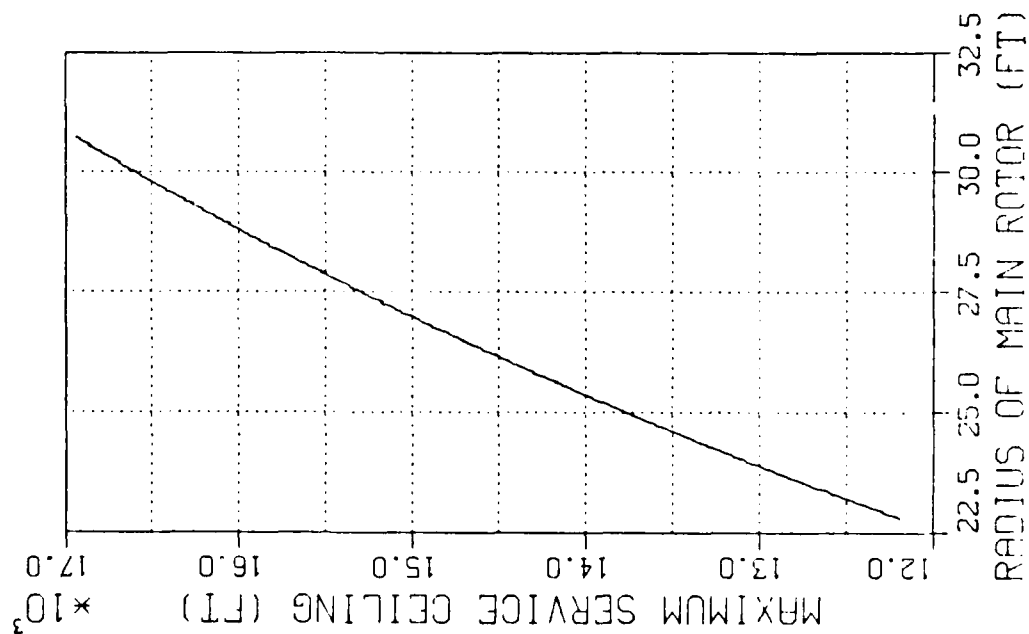


# ENDURANCE VELOCITY VERSUS RADIUS SOLIDITY, ADVANCE RATIO & TIP VELOCITY HELD CONSTANT CHORD & ROTATIONAL VELOCITY ALLOWED TO VARY WITH RADIUS

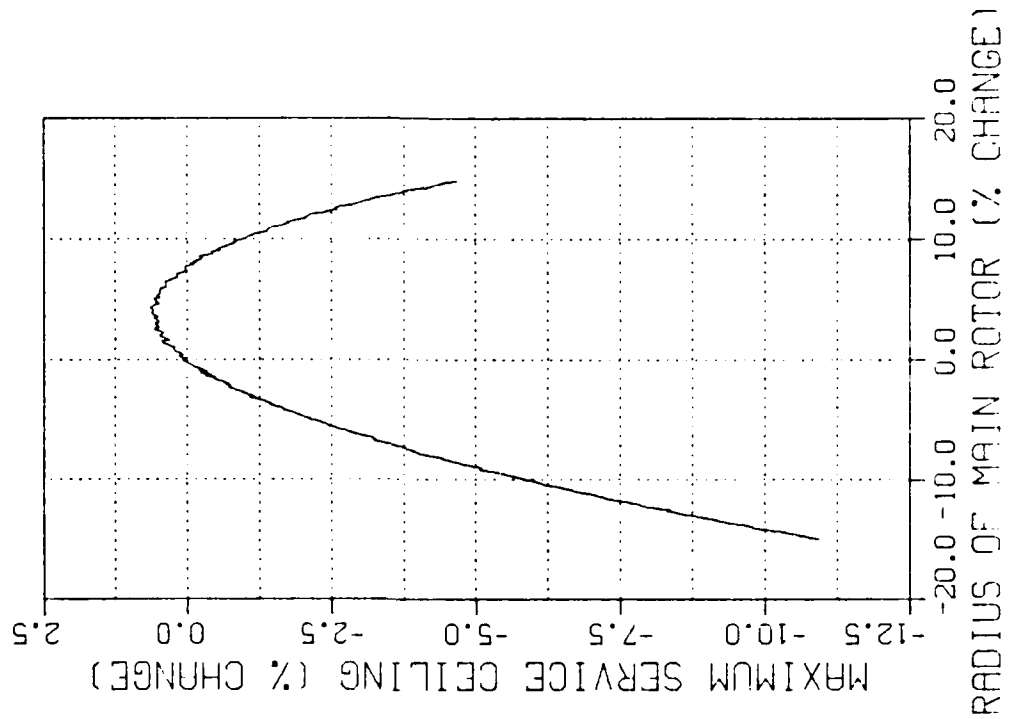
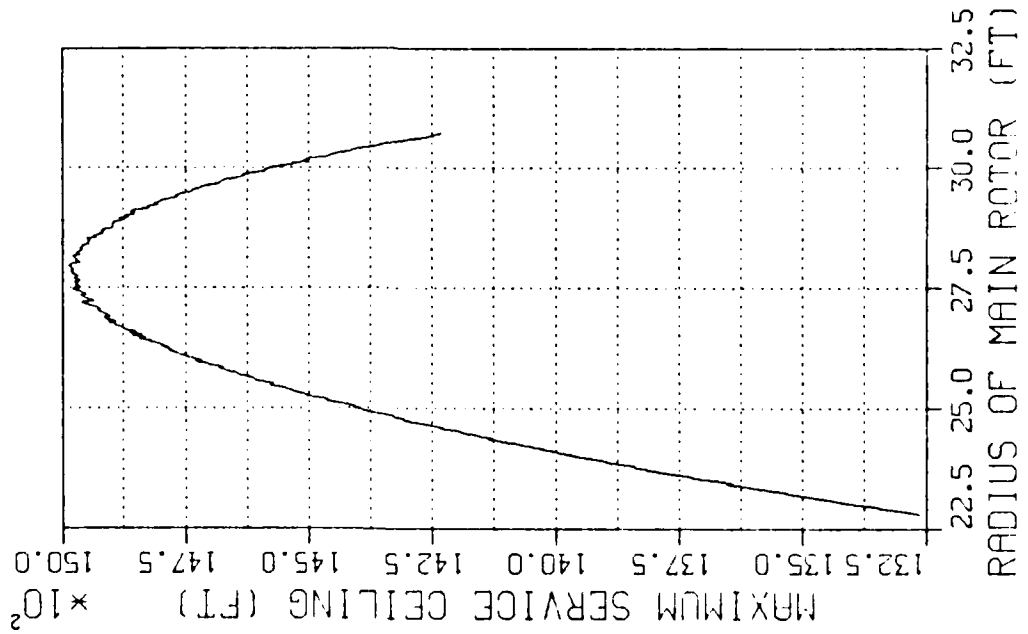




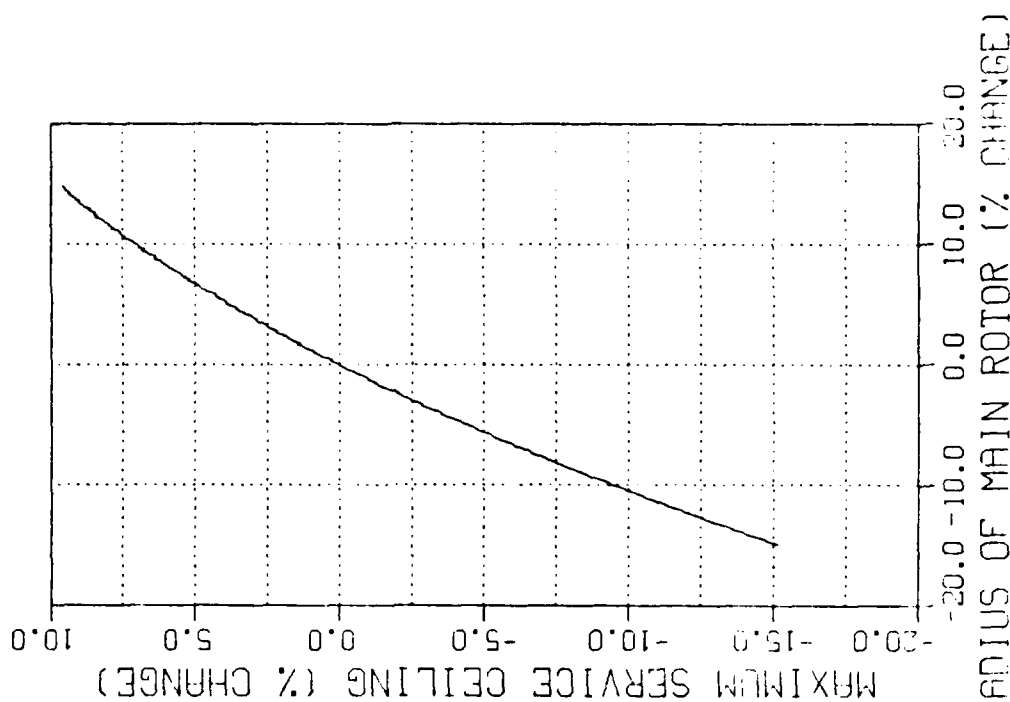
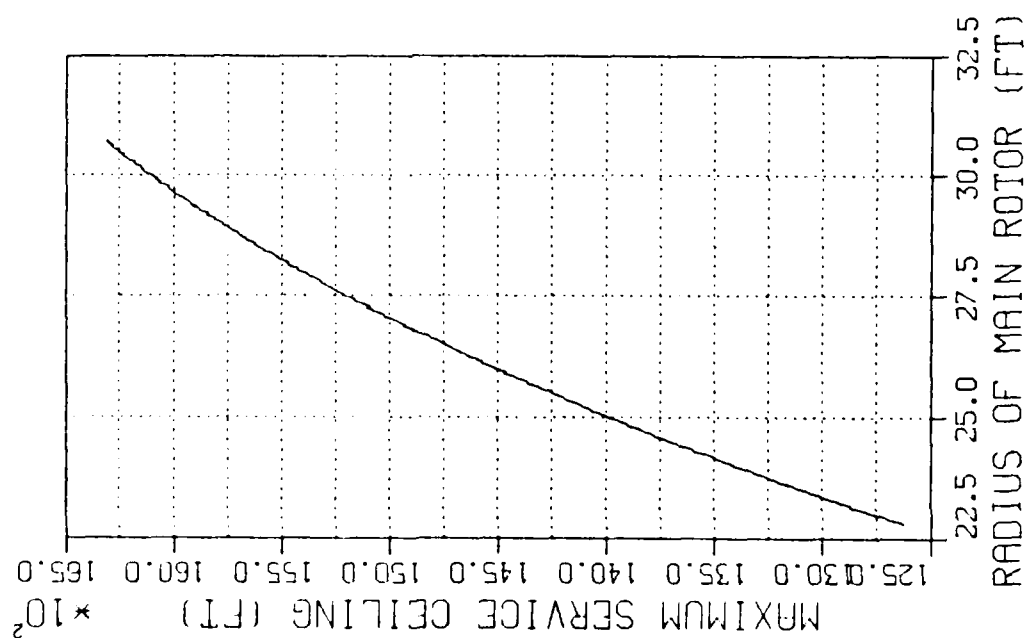
# MAXIMUM SERVICE CEILING VERSUS RADIUS CHANGE CHORD, TIP VELOCITY & ADVANCE RATIO HELD CONSTANT SOLIDITY, ROTATIONAL VELOCITY ALLOWED TO VARY WITH RADIUS



# MAXIMUM SERVICE CEILING VERSUS RADIUS CHANGE SOLIDITY & ROTATIONAL VELOCITY HELD CONSTANT CHORD, ADVANCE RATIO & TIP VELOCITY ALLOWED TO VARY WITH RADIUS



# MAXIMUM SERVICE CEILING VERSUS RADIUS CHANGE SOLIDITY, ADVANCE RATIO & TIP VELOCITY HELD CONSTANT CHORD & ROTATIONAL VELOCITY ALLOWED TO VARY WITH RADIUS



PEROCC10  
PEROCC20  
PEROCC30  
PEROCC40  
PEROCC50  
PEROCC60  
PEROCC70  
PEROCC80  
PEROCC90  
PEROCC100  
PEROCC110

# APPENDIX B

## COMPUTER PROGRAM LISTING

PEROCC170  
PEROCC180  
PEROCC190  
PEROCC200  
PEROCC210  
PEROCC220  
PEROCC230  
PEROCC240  
PEROCC250  
PEROCC260  
PEROCC270

### PERFORMANCE DESIGN PROGRAM COMPUTER PROGRAM LISTING

\*\*\*\*\*  
THIS PROGRAM WILL TAKE A SET OF HELICOPTER DESIGN DATA, RANGE  
CALCULATE POWER REQUIRED, ENDURANCE VELOCITY, RATE OF CLIMB, RANGE  
VELOCITY, POWER CEILING AND SERVICE CEILING FOR THAT DATA. IT  
ALSO WILL CALCULATE THE PERFORMANCE FACTORS LISTED ABOVE OVER A  
RANGE OF VALUES FOR THE GIVEN DATA. IT THEN WILL PLCT THE RESULTS  
VERSUS MAIN ROTOR RADIUS IN TWO FORMS. FORM 1 BEING THE PERFORMANCE  
FACTOR AT THE GIVEN SPECIFICATION VALUE VERSUS THE PERCENT  
DIFFERENCE OF THE RADIUS TO THE SPECIFICATION RADIUS.  
\*\*\*\*\*

TC RUN THE PROGRAM FLLCW THESE STEPS:

1. INPLT THE REQUIRED DATA IN LINES 175-207
2. COMPILE PROGRAM USING: FORTFX PERFORM (NOMAP  
NOTE: IF YOU DO NOT USE (NOMAP, YOU WILL NOT HAVE ENOUGH DISK  
SPACE TO RUN THE PROGRAM
3. GRAFF PRGGRAM USING: DISSPLA PERFORM
4. EXAMINE RESULTS BY USING: DISSPCF

\*\*\*\*\* DEFINITION OF TERMS \*\*\*\*\*

AHAT - ZERC HORSEPOWER FUEL FLOW INTERCEPT  
AMR - DISK AREA OF THE MAIN ROTOR (FT\*2)  
ARMR - ADVANCE RATIO OF THE MAIN ROTOR SYSTEM  
AKTR - ADVANCE RATIO OF THE TAIL ROTOR SYSTEM  
ATR - DISK AREA OF THE TAIL ROTOR (FT\*2)  
EHAT - AVERAGE SLOPE OF THE FUEL FLOW VS HORSEPOWER  
EUCMR - AVERAGE COEFFICIENT OF DRAG OF THE MAIN ROTOR BLADES  
CDCTR - AVERAGE COEFFICIENT OF DRAG OF THE TAIL ROTOR  
CEIL - SUBROUTINE TO CALCULATE MAX SERVICE CEILING  
CMA, CMRI - CHORD LENGTH OF MAIN ROTOR (FT)  
CONST - SUBROUTINE TO CALCULATE COMMON USED CONSTANTS  
CTMR - COEFFICIENT OF THRUST OF THE MAIN ROTOR SYSTEM  
CTTR - COEFFICIENT OF THRUST OF THE TAIL ROTOR SYSTEM  
C... - COEFFICIENT INDICATE A DIFFERENCE IN A VARIABLE, SEE VARIABLE  
DA - DENSITY ALTITUDE (FT)  
DELTA - PRESSURE RATIO (ALTITUDE/SSL)





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PERO1450  

PERO1460  

PERO1470  

PERO1480  

PERO1490  

PERO1500  

PERO1510  

PERO1520  

PERO1530  

PERO1540  

PERO1550  

PERO1560  

PERO1570  

PERO1580  

PERO1590  

PERO1600  

PERO1610  

PERO1620  

PERO1630  

PERO1640  

PERO1650  

PERO1660  

PERO1670  

PERO1680  

PERO1690  

PERO1700  

PERO1710  

PERO1720  

PERO1730  

PERO1740  

PERO1750  

PERO1760  

PERO1770  

PERO1780  

PERO1790  

PERO1800  

PERO1810  

PERO1820  

PERO1830  

PERO1840  

PERO1850  

PERO1860  

PERO1870  

PERO1880  

PERO1890  

PERO1900  

PERO1910  

PERO1920
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EFPAF = 25.7
EFPAV = 31.8
RTHT = 11.2
----- INPUT ENGINE DATA -----
IENG = 2
SFCM = C.46
SFCN = C.47
SFCC = C.51
SHPM = 1561.0
SHPN = 1218.0
SHPC = 589.0
----- INPUT FLIGHT VELOCITY FOR INITIAL POWER CALCULATIONS -----
VF1 = 50.0
===== END OF REQUIRED INPUT INFORMATION =====
C=====
DO 3000 K = 1,4
VV1 = C.C
PA = 0.0
TEMP = C.0
DA = 0.0
DENSSL = 0.00237694
SKDHT = 250C.0
VF = VF1
VV = VV1
CMR = CMR1
RVMR = FVMR1
PIE = 3.141593
SDMR3 = 18MR*CMR1 / (PIE*RADIUS)
VTMR2 = RVMR1*RADIUS
CALL RHC
CALL RAC (DIFF, RADIUS, RRMR, RMR, DRMR, MINZ, MAXZ, DMIN, DMAX)
IF (IANS.NE. 1) GO TO 2800
CALL PCWER
GO TO 3000
2800 IF (IANS.NE. 2) GO TO 2810
CALL ENCLR
GO TO 3000
2810 IF (IANS.NE. 3) GO TO 2820
CALL ENCLR
CALL MAXFC
GO TO 3000
2820 IF (IANS.NE. 4) GO TO 2830
CALL RANGE
GO TO 3000
2830 IF (IANS.NE. 5) GO TO 2840
CALL HCOVER
GO TO 3000
2840 IF (IANS.NE. 6) GO TO 2850

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PER01530
PER01540
PER01550
PER01560
PER01570
PER01580
PER01590
PER02000
PER02010
PER02020
PER02030
PER02040
PER02050
PER02060
PER02070
PER02080
PER02090
PER02100
PER02110
PER02120
PER02130
PER02140
PER02150
PER02160
PER02170
PER02180
PER02190
PER02200
PER02210
PER02220
PER02230
PER02240
PER02250
PER02260
PER02270
PER02280
PER02290
PER02300
PER02310
PER02320
PER02330
PER02340
PER02350
PER02360
PER02370
PER02380
PER02390
PER02400

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2850 CALL ENCLR
3000 CALL CEIL
5000 GO TO 3000
CONTINUE
CALL DCNEPL
CONTINUE
STOP
END
C*****
C      SUBROUTINES USED IN PRGRAM FULLCW
C*****
C      SUBROUTINE RAD(DIFF,RADIUS,RRMR,RMR,DRMR,MINZ,MAXZ,DMIN,DMAX)
C      IMPLICIT REAL (A-H,L-Z)
C      DIMENSION RMR(400),DRMR(400)
C      RMR = RADIUS - DIFF
C      DO 10 I = 1,324
C        RMR(I) = RRMR
C        IF (I.EQ.163) RMR(I) = RADIUS
C        RRMR = RRMR + DIFF/162
C      CONTINUE
C      DO 20 I = 1,324
C        DRMR(I) = ((RMR(I) - RMR(163)) / RMR(163)) * 100.0
C      CONTINUE
C      DMIN = DRMR(1)
C      DMAX = DRMR(324)
C      MINZ = RMR(1)
C      MAXZ = RMR(324)
C      RETURN
C      END
C*****
C      SUB-GROUP B
C      PERFORMANCE SUBROUTINES
C*****
C      SUBROUTINE TO CALCULATE ALL PARTS OF THE TOTAL POWER REQUIREMENTS
C      AND FIGURE OF MERIT.
C*****
C      SUBROUTINE POWER
C      IMPLICIT REAL (A-H,L-Z)

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PERO2410
PERO2420
PERO2430
PERO2440
PERO2450
PERO2460
PERO2470
PERO2480
PERO2490
PERO2500
PERO2510
PERO2520
PERO2530
PERO2540
PERO2550
PERO2560
PERO2570
PERO2580
PERO2590
PERO2600
PERO2610
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PERO2760
PERO2770
PERO2780
PERO2790
PERO2800
PERO2810
PERO2820
PERO2830
PERO2840
PERO2850
PERO2860
PERO2870
PERO2880

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INTEGER I,J,K
COMMON /A/ AMR, ARMR, ARTR, ATR, CDDMR, CDDTR, CMR, CTMR, CTR, CTTR,
* DA, DEN, EEPAF, EEPV, GE, HD, LPA, RADILS, RTR, RIHT, RVMR, RVTR, SLMR,
* SCIR, SKLHT, TEMP, W, VF, VV, VVIR, IBMR, DENSSL, PIE, PTMIN(400), VIMR,
* VITR, VITR, VIMR, RANMAX, THETA, DELTA, SHPRAN(400), VV1, VV1, IENG, SUMR3,
* VIMR2, LIFF, SFCM, SFCN, SFCC, SHPN, SHFN, SFFC, CMRI, RVMRI, RRRMR,
* CCMCN /B/ PIMR(400), PCMR(400), PPMR(400), PCMR(400), PITR(400),
* POTR(400), PTMR(400), PTTR(400), PTAC(400)
* CCMCN /C/ RMR(400), I, J, K, DRMR(400), MINX, MAXX, MINY, MAXY, MINZ,
* MAXZ, CMIN, DMAX, MINE, MAXB, MINC, MAXC, MIN, MAX, MAXA, IANS, TEXT(200)
COMMON /K/ RCMAX(400), DRCMAX(400), VFRAN(400), DVFRAN(400),
* HCVALT(400), DHVAL(400), SEVALT(400), DSEVAL(400), FMERT(400),
* OFMERT(400), VFEND(400), DVEND(400)
COMMON /Y/ DPIMR(400), DPMR(400), DPPMR(400), DPCMR(400), DPTMR(400),
* DPIR(400), DPOTR(400), DPTAC(400), DPTTR(400)
C-----
MAX = 0.0
MAXA = 0.0
DO 40 I = 1,324
CALL CONST
AMR = RMR(I) * 2.0 * PIE
IF(K .NE. 1) GO TO 8
      VMR = RVMR * RMR(I)
      ARMR = VF / (RVMR * RMR(I))
      SLMR = IBMR * CMR / (PIE * RMR(I))
8      IF(K .NE. 2) GO TO 10
      VMR = VTMR2 / RMR(I)
      VIMR = RVMR * RMR(I)
      ARMR = VF / (RVMR * RMR(I))
      SLMR = IBMR * CMRI / (PIE * RMR(I))
10     IF(K .NE. 3) GO TO 12
      CMR = SDMR3 * PIE * RMR(I) / IBMR
      SLMR = IBMR * CMR / (PIE * RMR(I))
      RVMR = RVMRI
      ARMR = VF / (RVMR * RMR(I))
      VIMR = RVMR * RMR(I)
12     IF(K .NE. 4) GO TO 14
      CMR = SDMR3 * PIE * RMR(I) / IBMR
      SLMR = IBMR * CMR / (PIE * RMR(I))
      VIMR = VTMR2 / RMR(I)
      VIMR = RVMR * RMR(I)
      ARMR = VF / (RVMR * RMR(I))
14     CALL VELMR
      CALL FCWMR
      CALL VELTR
      CALL FCWTR
      IF(FIMR(I)) .GT. MAXA) MAXA = PIMR(I)
      IF(FCMR(I)) .GT. MAXA) MAXA = PCMR(I)
PERO2890
PERO2900
PERO2910
PERO2920
PERO2930
PERO2940
PERO2950
PERO2960
PERO2970
PERO2980
PERO2990
PERO3000
PERO3010
PERO3020
PERO3030
PERO3040
PERO3050
PERO3060
PERO3070
PERO3080
PERO3090
PERO3100
PERO3110
PERO3120
PERO3130
PERO3140
PERO3150
PERO3160
PERO3170
PERO3180
PERO3190
PERO3200
PERO3210
PERO3220
PERO3230
PERO3240
PERO3250
PERO3260
PERO3270
PERO3280
PERO3290
PERO3300
PERO3310
PERO3320
PERO3330
PERO3340
PERO3350
PERO3360

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20      IF (FFMR(I) .GT. MAXA) MAXA = PPMR(I)
      IF (VV .LE. 0.0) GO TO 20
      IF (FCMR(I) .GT. MAXA) MAXA = PCMR(I)
      IF (PTAC(I) .GT. MAX) MAX = PTAC(I)
      VF = VF / 1.6885
      VV = VV * 60.0
40      CONTINUE
      MINV = 500.0
      MAXY = -500.0
      MINX = 500.0
      MAXX = -500.0
      DO 140 I = 1, 324
        CPIMR(I) = ((PIMR(I) - PIMR(163)) / PIMR(163)) * 100.0
        IF (CPIMR(I) .GT. MAXX) MAXX = CPIMR(I)
        IF (CPIMR(I) .LT. MINX) MINX = CPIMR(I)
        DPMF(I) = ((POMR(I) - POMR(163)) / POMR(163)) * 100.0
        IF (DPMF(I) .GT. MAXX) MAXX = DPMF(I)
        IF (DPMF(I) .LT. MINX) MINX = DPMF(I)
        DPPMR(I) = ((PPMR(I) - PPMR(163)) / PPMR(163)) * 100.0
        IF (DPPMR(I) .GT. MAXX) MAXX = DPPMR(I)
        IF (DPPMR(I) .LT. MINX) MINX = DPPMR(I)
        IF (VV .LE. 0.0) GO TO 120
        EPCMR(I) = ((PCMR(I) - PCMR(163)) / PCMR(163)) * 100.0
        IF (EPCMR(I) .GT. MAXX) MAXX = EPCMR(I)
        IF (EPCMR(I) .LT. MINX) MINX = EPCMR(I)
        DPTMR(I) = ((PTMR(I) - PTMR(163)) / PTMR(163)) * 100.0
        DPTTR(I) = ((PTTR(I) - PTTR(163)) / PTTR(163)) * 100.0
        DPTTF(I) = ((PTTF(I) - PTTF(163)) / PTTF(163)) * 100.0
        DPTAC(I) = ((PTAC(I) - PTAC(163)) / PTAC(163)) * 100.0
        IF (DPTAC(I) .GT. MAXY) MAXY = DPTAC(I)
        IF (DPTAC(I) .LT. MINY) MINY = DPTAC(I)
        IF (DPTMR(I) .GT. MAXY) MAXY = DPTMR(I)
        IF (DPTMR(I) .LT. MINY) MINY = DPTMR(I)
        IF (DPTTR(I) .GT. MAXY) MAXY = DPTTR(I)
        IF (DPTTR(I) .LT. MINY) MINY = DPTTR(I)
140      CONTINUE
      CALL GRAFIC
      CALL GRAFID
      VF = 0.0
      MINB = 1.0
      MAXB = 0.0
      DO 150 I = 1, 324
        CALL CCNST
        AMR = RMNR(I) * 2.0 * PIE
        IF (K .NE. 1) GO TO 142

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PERO3370
PERO3380
PERO3390
PERO3400
PERO3410
PERO3420
PERO3430
PERO3440
PERO3450
PERO3460
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PERO3480
PERO3490
PERO3500
PERO3510
PERO3520
PERO3530
PERO3540
PERO3550
PERO3560
PERO3570
PERO3580
PERO3590
PERO3600
PERO3610
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PERO3630
PERO3640
PERO3650
PERO3660
PERO3670
PERO3680
PERO3690
PERO3700
PERO3710
PERO3720
PERO3730
PERO3740
PERO3750
PERO3760
PERO3770
PERO3780
PERO3790
PERO3800
PERO3810
PERO3820
PERO3830
PERO3840

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142      VIMR = RVMR*RM(R(I))
      ARMR = VF / (RVMR*RM(R(I)))
      SCMR = IBMR*CMR / (PIE*RM(R(I)))
      IF(K.NE.2) GO TO 144
      VIMR = VIMR2/RM(R(I))
      ARMR = RVMR*RM(R(I))
      SCMR = VF / (RVMR*RM(R(I)))
      IF(K.NE.3) GO TO 146
      CMR = SDMR3*PIE*RM(R(I))/IBMR
      SCMR = IBMR*CMR / (PIE*RM(R(I)))
      RVMR = RVMR1
      ARMR = VF / (RVMR*RM(R(I)))
      VIMR = RVMR*RM(R(I))
      IF(K.NE.4) GO TO 148
      CMR = SDMR3*PIE*RM(R(I))/IBMR
      SDMR = IBMR*CMR / (PIE*RM(R(I)))
      RVMR = VIMR2/RM(R(I))
      VIMR = RVMR*RM(R(I))
      ARMR = VF / (RVMR*RM(R(I)))
      CALL VELMR
      CALL POWMR
      CALL VELTR
      CALL FCWTR
      FMERT(I) = PIMR(I) / (PIMR(I) + PCMR(I))
      IF(FMERT(I) -GT. MAXB) MAXB = FMERT(I)
      IF(FMERT(I) -LT. MINB) MINB = FMERT(I)
      IF(FMERT(I) -LT. MINC) MINC = FMERT(I)
      CONTINUE
150      MINC = 500.0
      MAXC = -500.0
      DO 155 I = 1,324
      FMERT(I) = ((FMERT(I) - FMERT(163)) / FMERT(163)) * 100.0
      IF(CFMERT(I) -GT. MAXC) MAXC = CFMERT(I)
      IF(CFMERT(I) -LT. MINC) MINC = CFMERT(I)
      CONTINUE
155      CALL GRAFLE
      RETURN
      END
C*****
C      SUBROUTINE TO CALCULATE THE ENDURANCE VELCCITY
C*****
C      SUBROUTINE ENDUR
C*****
C      IMPLICIT REAL (A-H,L-Z)
C      COMMON /A/ AMR, ARMR, ARTR, ATR, CCMR, CDOTR, CMR, CTR, CTRR,
PER03850
PER03860
PER03870
PER03880
PER03890
PER03900
PER03910
PER03920
PER03930
PER03940
PER03950
PER03960
PER03970
PER03980
PER03990
PER04000
PER04010
PER04020
PER04030
PER04040
PER04050
PER04060
PER04070
PER04080
PER04090
PER04100
PER04110
PER04120
PER04130
PER04140
PER04150
PER04160
PER04170
PER04180
PER04190
PER04200
PER04210
PER04220
PER04230
PER04240
PER04250
PER04260
PER04270
PER04280
PER04290
PER04300
PER04310
PER04320

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* DA, DEN, EFPAF, EFPV, GE, HD, L, PA, RADILS, RTR, RIHT, RVMR, RVTR, SCDR,
* SCTR, SKCHT, TEMP, W, VF, VV, IBTR, IBMR, CENSSL, PIE, PTMIN(400), VIMR,
* VITR, VITR, VIMR, RANMAX, THETA, DELTA, SHPRAN(400), VVI, VFI, IENG, SCDMR3,
* VIMR2, CIFF, SFCC, SHPM, SHPN, SHFC, CMR1, RVMR1, RMR
* CCMCN /B/ PIMR(400), PQMR(400), PPMR(400), PTAC(400),
* POTR(400), PTIR(400), PTAC(400)
* CCMCN /C/ RMR(400), I, J, K, DRMR(400), MINX, MAXX, MINY, MAXY, MINZ,
* MAXZ, MIN, DMAX, MINB, MAXB, MINC, MAXC, MIN, MAX, MAXA, IANS, TEXT(200),
* CCMCN /W/ RCMAX(400), DRCMAX(400), VFRAN(400), DVFRAN(400),
* HCVALT(400), DHOVAL(400), SEVALT(400), DSEVAL(400), FMEKT(400),
* DFMEKT(400), VFEND(400), DVFEND(400)
* CCMCN /Z/ VFEND1(400), VFEND2(400), VFEND3(400), VFEND4(400)
C-----
MAX = C.C
MIN = 500.0
CALL RHC
DO 280 I = 1, 324
  AMR = RMR(I)*2 - 0*PIE
  IF(K .NE. 1) GO TO 148
    RVMR = RVMR1 RMR(I)
    SCMR = IBMR*CMR / (PIE*RMR(I))
  148 IF(K .NE. 2) GO TO 150
    RVMR = VIMR2/RMR(I)
    SCMR = RVMR*CMR(I)
  150 IF(K .NE. 3) GO TO 152
    SCMR = IBMR*CMR1 / (PIE*RMR(I))
    CMR = SCDMR3*PIE*RMR(I)/IBMR
    SCMR = IBMR*CMR / (PIE*RMR(I))
    RVMR = RVMR1 RMR(I)
    VIMR = RVMR*CMR(I)
  152 IF(K .NE. 4) GO TO 154
    CMR = SCDMR3*PIE*RMR(I)/IBMR
    SCMR = IBMR*CMR / (PIE*RMR(I))
    RVMR = VIMR2/RMR(I)
    VIMR = RVMR*CMR(I)
  154 PTMIN(I) = 1000.0
    VFEND(I) = 0.0
    DO 180 J = 1, 20
      VF = FLOAT(J) * 10.0
      CALL CONST
      ARMR = VF / (RVMR*RMR(I))
      CALL VELMR
      CALL POWMR
      CALL VELTR
      CALL POWTR
      IF (PTAC(I) .GT. PTMIN(I)) GO TO 160
      PTMIN(I) = PTAC(I)

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160 VFEND(I) = VF/1.68889
180 CCNTINUE
CONTINUE
VFEND(I) = VFEND(I) - 10.0
VFF = VFEND(I)
DO 220 J = 1,20
VF = (FLGAT(J)-1.0) + VFF
CALL CONST
ARMR = VF / (RVMR*RM(R))
CALL VELMR
CALL POWMR
CALL VELTR
CALL POWTR
IF (PTAC(I) -GT. PTMIN(I)) GC TC 200
PTMIN(I) = PTAC(I)
VFEND(I) = VF/1.68889
CCNTINUE
200 CONTINUE
VFEND(I) = VFEND(I) - 1.0
VFF = VFEND(I)
DO 260 J = 1,200
VF = ((FLGAT(J)/100)-0.01) + VFF
CALL CONST
ARMR = VF / (RVMR*RM(R))
CALL VELMR
CALL POWMR
CALL VELTR
CALL POWTR
IF (PTAC(I) -GT. PTMIN(I)) GC TC 240
PTMIN(I) = PTAC(I)
VFEND(I) = VF/1.68889
CCNTINUE
240 CONTINUE
VFEND(I) = VFEND(I) - 0.01
IF (K.EQ. 1) VFEND1(I) = VFEND(I)
IF (K.EQ. 2) VFEND2(I) = VFEND(I)
IF (K.EQ. 3) VFEND3(I) = VFEND(I)
IF (K.EQ. 4) VFEND4(I) = VFEND(I)
IF (VFEND(I) .LT. MIN) MIN = VFEND(I)
IF (VFEND(I) .GT. MAX) MAX = VFEND(I)
CCNTINUE
260 CONTINUE
MAXY = -500.0
MINY = 500.0
DO 280 I = 1,324
DVVFEND(I) = ((VFEND(I) - VFEND(163)) / VFEND(163)) * 100.0
IF (CVVFEND(I) .GT. MAXY) MAXY = CVVFEND(I)
IF (CVVFEND(I) .LT. MINY) MINY = CVVFEND(I)
280 CONTINUE

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PER04810
PER04820
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PER04900
PER04910
PER04920
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PER04940
PER04950
PER04960
PER04970
PER04980
PER04990
PER05000
PER05010
PER05020
PER05030
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PER05080
PER05090
PER05100
PER05110
PER05120
PER05130
PER05140
PER05150
PER05160
PER05170
PER05180
PER05190
PER05200
PER05210
PER05220
PER05230
PER05240
PER05250
PER05260
PER05270
PER05280

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[illegible]









PER09130  
PER09140  
PER09150  
PER09160  
PER09170  
PER09180  
PER09190  
PER09200  
PER09210  
PER09220  
PER09230  
PER09240  
PER09250  
PER09260  
PER09270  
PER09280  
PER09290  
PER09300  
PER09310  
PER09320  
PER09330  
PER09340  
PER09350  
PER09360  
PER09370  
PER09380  
PER09390  
PER09400  
PER09410  
PER09420  
PER09430  
PER09440  
PER09450  
PER09460  
PER09470  
PER09480  
PER09490  
PER09500  
PER09510  
PER09520  
PER09530  
PER09540  
PER09550  
PER09560  
PER09570  
PER09580  
PER09590  
PER09600

```

VF = VFF
LA = FLOAT(J)*1000.0
CALL RHO
VV = 100.0
CALL CONST
ARMR = VF / (RVMR*RRMR(I))
CALL VELMR
CALL POWMR
CALL VELTR
CALL POWTR
FCWAA = PTAVL*DELTA*SQR(THETA)
IF (PTAC(I) .LT. POWAA) GO TC 1420
SEVALT(I) = CA
GO TO 1440
CCNTINUE
CONTINUE
SEV = SEVALT(I) - 1000.0
DO 1460 J = 1,20
VF = VFF
LA = FLOAT(J)*50.0 + SEV
CALL RHC
VV = 100.0
CALL CONST
ARMR = VF / (RVMR*RRMR(I))
CALL VELMR
CALL POWMR
CALL VELTR
CALL POWTR
FCWAA = PTAVL*DELTA*SQR(THETA)
IF (PTAC(I) .LT. POWAA) GO TC 1460
SEVALT(I) = CA
GO TO 1480
CCNTINUE
CONTINUE
SEV = SEVALT(I) - 50.0
DO 1480 J = 1,100
VF = VFF
LA = FLOAT(J)*0.5 + SEV
CALL RHO
VV = 100.0
CALL CONST
ARMR = VF / (RVMR*RRMR(I))
CALL VELMR
CALL POWMR
CALL VELTR
CALL POWTR
FCWAA = PTAVL*DELTA*SQR(THETA)
IF (PTAC(I) .LT. POWAA) GO TC 1500

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1420  
1440

1460  
1480

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C*****
SUBROUTINE CEIL (A-H, L-Z)
IMPLICIT REAL (A-H, L-Z)
COMMON /A/ AMR, ARTR, ATR, CDCMR, CDOIR, CMR, CTMR, CTR, CTTR, SDMR,
DA, DEN, EFAF, EFPV, GE, HD, L, PA, RADILS, RTR, RTHI, RVMR, RVTR, SDMR,
SDTR, SKCHT, IEMP, W, VF, VV, IBTR, IBMR, DENSSL, PIE, PTMIN(400), VIMR,
VITR, VITR, VIMR, RANMAX, THETA, DELTA, SHPRAN(400), VV1, VF1, IENG, SDMR3,
VITR2, CIFF, SFCM, SFCN, SFCR, SHPN, SHPN, SHFC, CRI, RVMR1, RMR,
CCMMCN /B/ PTMR(400), POMR(400), PCMR(400), PITR(400),
PTR(400), PTTR(400), PTAC(400)
CCMMCN /C/ RMTR(400), I, J, K, DRMR(400), MINX, MAXX, MINY, MAXY, MINZ,
MAXZ, DMIN, DMAX, MINB, MAXB, PINC, MAXC, MIN, MAX, IANS, TEXT(200),
COMMON /A/ RCMAX(400), DRCMAX(400), VFRAN(400), DVFRAN(400),
HCVALT(400), DHOVAL(400), SEVALT(400), DSEVAL(400), FMERT(400),
FMERT(400), VFEND(400), DVFEND(400)
CCMMCN /Z/ VFEND1(400), VFEND2(400), VFEND3(400), VFEND4(400)
C-----
SKCHT = 2500.0
MIN = 30000.0
MAX = 0.0
PA = 0.0
TEMP = 0.0
IF (IENG .EQ. 1) PTAVAI = (FLOAT(IENG)*SHPN - 10.0) * 0.97
IF (IENG .EQ. 2) PTAVAI = (FLOAT(IENG)*SHPN - 10.0) * 0.9#0.97
IF (IENG .EQ. 3) PTAVAI = (FLOAT(IENG)*SHPN - 10.0) * 0.9#0.94
DO 154C I = 1, 324
AMR = RMTR(I)*2.0*PIE
IF (K .NE. 1) GC TC 1408
VFF = VFEND1(I)
VTMR = RVMR1*RMTR(I)
SDMR = IBMR*CMR1 / (PIE*RMTR(I))
IF (K .NE. 2) GO TO 1412
VFF = VFEND2(I)
VTMR = VTMR2/RMR(I)
SDMR = IBMR*CMR1 / (PIE*RMTR(I))
IF (K .NE. 3) GO TO 1414
VFF = VFEND3(I)
CMR = SDMR3*PIE*RMTR(I)/IBMR
SDMR = IBMR*CMR / (PIE*RMTR(I))
VTMR = RVMR1*RMTR(I)
IF (K .NE. 4) GO TO 1416
CMR = SDMR3*PIE*RMTR(I)/IBMR
SDMR = IBMR*CMR / (PIE*RMTR(I))
VTMR = RVMR2/RMR(I)
VFF = VFEND4(I)
CO 1420 J = 1, 30

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PER08650
PER08660
PER08670
PER08680
PER08690
PER08700
PER08710
PER08720
PER08730
PER08740
PER08750
PER08760
PER08770
PER08780
PER08790
PER08800
PER08810
PER08820
PER08830
PER08840
PER08850
PER08860
PER08870
PER08880
PER08890
PER08900
PER08910
PER08920
PER08930
PER08940
PER08950
PER08960
PER08970
PER08980
PER08990
PER09000
PER09010
PER09020
PER09030
PER09040
PER09050
PER09060
PER09070
PER09080
PER09090
PER09100
PER09110
PER09120

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COMMON /W/ RCMAX(400), DRCMAX(400), VFRAN(400), DVFRAN(400),
* HCVALT(400), DHOVAL(400), SEVALT(400), DSEVAL(400), FMERT(400),
* DFMEKT(400), VFEND(400), DVFEND(400)

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```

C-----
VF = 0.0
VV = 0.0
SKCHT = 10.0
MIN = 3000.0
MAX = 0.0
PA = 0.0
TEMP = 0.0
IF (IENG.EQ.1) PTAVAL = (FLOAT(IENG)*SHPN - 10.0) * 0.97
IF (IENG.EQ.2) PTAVAL = (FLOAT(IENG)*SHPN - 10.0) * 0.9 * C.97
IF (IENG.EQ.3) PTAVAL = (FLOAT(IENG)*SHPN - 10.0) * 0.9 * 0.94
DO 1240 I = 1, 324
  AMR = RMR(I) * 2.0 * PIE
  IF (K.NE.1) GO TO 1108
  VTMR = RMR1 * RMR(I) / (PIE * RMR(I))
  SDMR = IBMR * CMR1 / (PIE * RMR(I))
1108   IF (K.NE.2) GO TO 1112
  VTMR = VTMR2 / RMR(I)
  SDMR = VTMR * CMR1 / (PIE * RMR(I))
1112   IF (K.NE.3) GO TO 1114
  CMR = SDMR3 * PIE * RMR(I) / IBMR
  SLMR = IBMR * CMR / (PIE * RMR(I))
  VTMR = RMR1 * RMR(I)
1114   IF (K.NE.4) GO TO 1116
  CMR = SDMR3 * PIE * RMR(I) / IBMR
  SLMR = IBMR * CMR / (PIE * RMR(I))
  FVMR = VTMR2 / RMR(I)
  VTMR = RMR * RMR(I)
1116   ARMR = VF / (RVMR * RMR(I))
  DO 1120 J = 1, 30
    IA = FLOAT(J) * 1000.0
    CALL RHO
    CALL CUNST
    CALL VELMR
    CALL POWMR
    CALL VELTR
    CALL POWTR
    FCWAA = PTAVAL * DELTA * SQR(THETA)
    IF (PTAC(I) .LT. POWAA) GOTC 1120
    HCVALT(I) = CA
    GC TO 1140
  CCNTINUE
CONTINUE
HOV = HOVALT(I) - 1000.0
1120
1140

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PERO7690
PERO7700
PERO7710
PERO7720
PERO7730
PERO7740
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PERO7800
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PERO7970
PERO7980
PERO7990
PERO8000
PERO8010
PERO8020
PERO8030
PERO8040
PERO8050
PERO8060
PERO8070
PERO8080
PERO8090
PERO8100
PERO8110
PERO8120
PERO8130
PERO8140
PERO8150
PERO8160

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734      VTMR = RVMR1*RMNR(I)
      IF(K.NE.4) GO TO 736
      CMR = SDMR3*PIE*RMNR(I)/IBMR
      SDMR = IBMR*CMR / (PIE*RMNR(I))
      RVMR = VTMR2/RMR(I)
      VTMR = 1.20
      DO 740 J = 1,20
      VF = FLOCAT(J)*10.0
      CALL CONST
      ARMR = VF / (RVMR*RMNR(I))
      CALL VELMR
      CALL POWMR
      CALL VELTR
      CALL POWTR
      DE = 550.0*(PTAC(I)+PSHP) / VF
      WDE = W / DE
      IF (WDE.LE. RANMAX) GO TO 750
      RANMAX = WDE
      VFRAN(I) = VF/1.68885
      CONTINUE
740      CONTINUE
750      VFF = VFRAN(I)
      RANMAX = 0.0
      DO 820 J = 1,20
      VF = FLOCAT(J)-1.0 + VFF
      CALL CONST
      ARMR = VF / (RVMR*RMNR(I))
      CALL VELMR
      CALL POWMR
      CALL VELTR
      CALL POWTR
      LE = 550.0 * (PTAC(I)+PSHP) / VF
      IF(DE.EQ.0.0) GO TO 780
      WDE = W / DE
      GC TO 800
      WDE = 0.0
      IF (WDE.LT. RANMAX) GO TO 850
      RANMAX = WDE
      VFRAN(I) = VF/1.68885
      CONTINUE
820      CONTINUE
850      VFF = VFRAN(I)
      RANMAX = 0.0
      DO 880 J = 1,201
      VF = (FLOCAT(J-1)/100.0) + VFF
      CALL CONST
      ARMR = VF / (RVMR*RMNR(I))
      CALL VELMR

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PER06730
PER06740
PER06750
PER06760
PER06770
PER06780
PER06790
PER06800
PER06810
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PER06900
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PER06940
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PER06960
PER06970
PER06980
PER06990
PER07000
PER07010
PER07020
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PER07080
PER07090
PER07100
PER07110
PER07120
PER07130
PER07140
PER07150
PER07160
PER07170
PER07180
PER07190
PER07200

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PER05770  
 PER05780  
 PER05790  
 PER05800  
 PER05810  
 PER05820  
 PER05830  
 PER05840  
 PER05850  
 PER05860  
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 PER05880  
 PER05890  
 PER05900  
 PER05910  
 PER05920  
 PER05930  
 PER05940  
 PER05950  
 PER05960  
 PER05970  
 PER05980  
 PER05990  
 PER06000  
 PER06010  
 PER06020  
 PER06030  
 PER06040  
 PER06050  
 PER06060  
 PER06070  
 PER06080  
 PER06090  
 PER06100  
 PER06110  
 PER06120  
 PER06130  
 PER06140  
 PER06150  
 PER06160  
 PER06170  
 PER06180  
 PER06190  
 PER06200  
 PER06210  
 PER06220  
 PER06230  
 PER06240

```

492 IF(K .NE. 3) GO TO 494
    VF = VFEND3(I)
    CMR = SDMR3*PIE*RM(R(I))/IBMR
    SDCMR = IBMR*CMR / (PIE*RM(R(I)))
    VTMR = RM(R(I))*RM(R(I))
494 IF(K .NE. 4) GO TO 496
    VF = VFEND4(I)
    CMR = SDMR3*PIE*RM(R(I))/IBMR
    SDCMR = IBMR*CMR / (PIE*RM(R(I)))
    VTMR = RM(R(I))*RM(R(I))
496 DO 500 J = 1,80
    VV = FLOAT(J)*100.0
    CALL CONST
    ARMR = VF / (RVMR*RM(R(I)))
    CALL VELMR
    CALL POWMR
    CALL VELTR
    CALL POWTR
    IF (PTAC(I) .GT. PTAVAL) GO TO 520
    VF = VF/1.68889
    CONTINUE
500 RCMAXX = (VV*60.0) - 100.0
520 VF = VF/1.68889
    DO 540 J = 1,100
    VV = FLOAT(J)*1.0 + RCMAXX
    CALL CONST
    ARMR = VF / (RVMR*RM(R(I)))
    CALL VELMR
    CALL POWMR
    CALL VELTR
    CALL POWTR
    IF (PTAC(I) .GT. PTAVAL) GO TO 560
    VF = VF/1.68889
    CONTINUE
540 RCMAX(I) = (VV*60.0)-1.0
560 IF(RCMAX(I) .LT. MIN) MIN = RCMAX(I)
    IF(RCMAX(I) .GT. MAX) MAX = RCMAX(I)
    CONTINUE
580 -----
    MAXY = -500.0
    MINY = 500.0
    DO 700 I = 1,324
    DRCMAX(I) = ((RCMAX(I) - RCMAX(163)) / RCMAX(163)) * 100.0
    IF(DRCMAX(I) .GT. MAXY) MAXY = DRCMAX(I)
    IF(DRCMAX(I) .LT. MINY) MINY = DRCMAX(I)
    CONTINUE
700 CALL GRAF3
  
```

```

480 CONTINUE
IF(IANS.EQ.3.OR.IANS.EQ.6) GO TO 482
CALL GRAF2
CONTINUE
RETURN
ENC
C*****
C SUBROUTINE TO CALCULATE THE MAXIMUM RATE OF CLIMB
C*****
C SUEROUTINE MAXRC
C IMPLICIT REAL (A-H,L-Z)
COMMON /A/ AMR,ARTR,ATR,CDCMR,CDOIR,CMF,CTMR,CTR,CTTR,SDMR,
* DA,DEN,EFPF,EFPAF,GE,HD,L,PA,RADILS,RTR,RTHT,RVMR,RVTR,SDMR,
* SDTR,SKDHT,TEMP,W,VF,VV,IBTR,IBMR,DENSSL,PIE,PTMIN(400),VIMR,
* VITR,VITR,VIMR,RANMAX,THETA,DELTA,SHPRAN(400),VV1,VF1,IENG,SDMR3,
* VIMR2,LIFF,SFCM,SFCN,SFCC,SHPM,SHPN,SHFC,CPRI,RVMR1,RMR,
* COMMON /B/ PIMR(400),POMR(400),PPMR(400),PCMR(400),PITR(400),
* PCTR(400),PTMR(400),PTTR(400),PTAC(400)
* CCMCN /C/ RMR(400),I,J,K,DRMR(400),MINX,MAXX,MINY,MAXY,MINZ,
* MAXZ,CMIN,DMAX,MINB,MAXB,MINC,MAXC,MINMAX,MAXA,IANS
* COMMON /W/ RCMAX(400),CRCMAX(400),VFRAN(400),DVFRAN(400),
* HUVALT(400),DHQVAL(400),SEVALT(400),DSEVAL(400),FMERT(400),
* DFMERT(400),VFEND(400),DVEND(400)
* CCMCN /Z/ VFEND1(400),VFEND2(400),VFEND3(400),VFEND4(400)
C-----
PA = 0.0
TEMP = 0.0
DA = 0.0
IF(IENG.EQ.1) PTAVAL = (FLOAT(IENG)*SHPM - 10.0) * 0.97
IF(IENG.EQ.2) PTAVAL = (FLOAT(IENG)*SHPM - 10.0) * 0.9*0.97
IF(IENG.EQ.3) PTAVAL = (FLOAT(IENG)*SHPM - 10.0) * 0.9*0.94
CALL RFC
MAX = 800.0
DO I = 1,324
AMR = RMR(I)*#2,0*PIE
IF(K.NE.1) GC TO 490
VF = VFEND1(I)
VTMR = RVMR1/RMR(I)
SCMR = IBMR*CMR1 / (PIE*RMR(I))
IF(K.NE.2) GO TO 492
VF = VFEND2(I)
VTMR = VTMR2/RMR(I)
VTNR = RVMR*CMR1 / (PIE*RMR(I))
SCMR = IBMR*CMR1 / (PIE*RMR(I))
490

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CALL CHNCCT (DRMR,DPTMR,322,0)	PER12010
CALL CLNVE (DRMR,DPTAC,322,0)	PER12020
CALL CLNVE (DRMR,DPTAC,322,0)	PER12030
MAXLIN=LINEST(TEXT,100,30)	PER12040
CALL FLIGHT(0,1)	PER12050
CALL LINES(TAIL RCTOR POWER\$,TEXT,1)	PER12060
CALL LINES(MAIN RCTOR POWER\$,TEXT,2)	PER12070
CALL LINES(TOTAL POWER\$,TEXT,3)	PER12080
CALL LEGEND(TEXT,3,0.4,3.8)	PER12090
CALL BLREC(0.3,3.7,1.55,0.75,1.2)	PER12100
CALL RESET(HEIGHT)	PER12110
CALL DCT	PER12120
CALL GFC(1,2)	PER12130
CALL ENDCR(0)	PER12140
-----	PER12150
CALL PHYSOR(1.5,1.5)	PER12160
CALL AREA2D(6.50,4.70)	PER12170
CALL HEADIN(POWER VERSUS RADIUS\$,19,1.4,3)	PER12180
IF(K NE 1) GO TO 8	PER12190
* CALL HEADIN(CHORD & ROTATIONAL VELOCITY HELD CONSTANT\$,41,	PER12200
HEADIN(SOLIDITY, TIP VELOCITY & ADVANCE RATIO\$,38,0.8,4)	PER12210
CALL MESSAGE(ALLOWED TO VARY WITH RADIUS\$,27,0.8,4)	PER12220
CALL MESSAGE(SPEC RMR=\$,100,7.4,6.5)	PER12230
CALL REALNO(RMR(163),2,ABUT\$,ABLT\$)	PER12240
CALL MESSAGE(CASE 1\$,100,8.7,6.0)	PER12250
IF(K NE 2) GO TO 10	PER12260
* CALL HEADIN(CHORD,TIP VELOCITY & ADVANCE RATIO HELD CONSTANT\$,	PER12270
HEADIN(SOLIDITY, ROTATIONAL VELOCITY\$,29,0.8,4)	PER12280
CALL MESSAGE(ALLOWED TO VARY WITH RADIUS\$,27,0.8,4)	PER12290
CALL MESSAGE(SPEC RMR=\$,100,7.4,6.5)	PER12300
CALL REALNO(RMR(163),2,ABUT\$,ABLT\$)	PER12310
CALL MESSAGE(CASE 2\$,100,8.7,6.0)	PER12320
IF(K NE 3) GO TO 12	PER12330
* CALL HEADIN(SOLIDITY & ROTATIONAL VELOCITY HELD CONSTANT\$,	PER12340
HEADIN(CHORD,ADVANCE RATIO & TIP VELOCITY\$,34,0.8,4)	PER12350
CALL MESSAGE(ALLOWED TO VARY WITH RADIUS\$,27,0.8,4)	PER12360
CALL MESSAGE(SPEC RMR=\$,100,7.4,6.5)	PER12370
CALL REALNO(RMR(163),2,ABUT\$,ABLT\$)	PER12380
CALL MESSAGE(CASE 3\$,100,8.7,6.0)	PER12390
IF(K NE 4) GO TO 14	PER12400
* CALL HEADIN(SOLIDITY,ADVANCE RATIO & TIP VELOCITY HELD CONSTANT\$,	PER12410
HEADIN(CHORD & ROTATIONAL VELOCITY\$,27,0.8,4)	PER12420
CALL MESSAGE(ALLOWED TO VARY WITH RADIUS\$,27,0.8,4)	PER12430
CALL HEADIN(CHORD & ROTATIONAL VELOCITY\$,27,0.8,4)	PER12440
CALL HEADIN(CHORD & ROTATIONAL VELOCITY\$,27,0.8,4)	PER12450
CALL HEADIN(CHORD & ROTATIONAL VELOCITY\$,27,0.8,4)	PER12460
CALL HEADIN(CHORD & ROTATIONAL VELOCITY\$,27,0.8,4)	PER12470
CALL HEADIN(CHORD & ROTATIONAL VELOCITY\$,27,0.8,4)	PER12480



PER12570  
PER12580  
PER12590  
PER12600  
PER13010  
PER13020  
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PER13360  
PER13370  
PER13380  
PER13390  
PER13400  
PER13410  
PER13420  
PER13430  
PER13440

CALL BLREC(0.3,3.42,2.15,1.00,1.1)  
CALL RESET(HEIGHT)  
CALL DCT  
CALL GRID(1,2)  
CALL ENGR(0)

-----  
CALL PHYSOR(5.5,1.5)  
CALL AREA2D(2.50,4.50)  
CALL XNAME('RADIUS OF MAIN ROTCR (% CHANGE)',100)  
CALL YNAME('POWER REQUIRED (% CHANGE)',100)  
CALL GRAF(EMIN,SCALE,DMAX,MINX,SCALE,MAXX)  
CALL LEGLIN  
CALL CUFVE(DRMR,DPIMR,324,0)  
CALL DASH  
CALL CUFVE(DRMR,DPQMR,324,0)  
CALL CFNCOT  
CALL CURVE(DRMR,DPPMR,324,0)  
CALL CFNCOSH  
CALL CURVE(DRMR,DPITR,324,0)  
CALL DCT  
CALL CUFVE(DRMR,DFCTR,324,0)  
IF (VV.LE.0.0) GC TC 22  
CALL CUFVE(DRMR,DPCMR,322,0)  
MAXLIN=LINEST(TEXT,100,30)  
CALL HEIGHT(0.1)  
CALL LINES(INDUCED POWER (MR)\$,TEXT,1)  
CALL LINES(PROFILE POWER (MR)\$,TEXT,2)  
CALL LINES(PARASITE POWER (MR)\$,TEXT,3)  
CALL LINES(INDUCED POWER (TR)\$,TEXT,4)  
CALL LINES(PROFILE POWER (TR)\$,TEXT,5)  
CALL LEGEND(TEXT,5,0.4,3.50)  
CALL BLREC(0.3,3.42,2.2,1.00,1.2)  
CALL RESET(HEIGHT)  
CALL DCT  
CALL GRID(1,2)  
CALL ENGR(0)

22

84

-----  
CALL PHYSOR(1.5,1.5)  
CALL AREA2D(6.50,4.70)  
CALL HEACIN('POWER 8  
IF(K.NE.1) GO TC 8  
CALL HEACIN('CHORD & ROTATIONAL VELOCITY HELD CONSTANT',41,  
0.8,3)  
\*  
CALL HEACIN('SOLIDITY, TIP VELOCITY & ADVANCE RATIO',38,0.8,4)  
CALL HEACIN('ALLOWED TC VARY WITH RADIUS',27,0.8,4)  
CALL MESSAGE('SPEC RMR =',100,7.4,6.5)  
CALL REALNO(RMR(1.63),2,ABUT,ABUT)  
CALL MESSAGE('CASE 1',100,8.7,6.0)

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8      IF(K .NE. 2) GO TO 10
9      CALL HEADIN('CHCRC,TIP VELOCITY & ADVANCE RATIO HELD CONSTANT$',
10     *    4E,0.8,4)
11     CALL HEADIN('SOLICITY, ROTATIONAL VELOCITY$, 29,0.8,4)
12     CALL MESSAG('SPEC RMR =$, 100,7.4,6.5)
13     CALL REALNC(RMR(163),2,'ABUT','ABUT:')
14     CALL MESSAG('CASE 2$, 100,8.7,6.0)
15     IF(K .NE. 3) GO TO 12
16     CALL HEADIN('SOLIDITY & ROTATIONAL VELOCITY HELD CONSTANT$',
17     *    44,C.8,4)
18     CALL HEADIN('CHCRC,ADVANCE RATIO & TIP VELOCITY$, 24,0.8,4)
19     CALL MESSAG('ALLOWED TO VARY WITH RADIUS$, 27,0.8,4)
20     CALL REALNC(RMR(163),2,'ABUT','ABUT:')
21     CALL MESSAG('CASE 3$, 100,8.7,6.0)
22     IF(K .NE. 4) GO TO 14
23     CALL HEADIN('SOLIDITY,ADVANCE RATIO & TIP VELOCITY HELD CONSTANTS$',
24     *    51,0.8,4)
25     CALL HEADIN('CHCRC & ROTATIONAL VELOCITY$, 27,0.8,4)
26     CALL MESSAG('ALLOWED TO VARY WITH RADIUS$, 27,0.8,4)
27     CALL REALNC(RMR(163),2,'ABUT','ABUT:')
28     CALL MESSAG('CASE 4$, 100,8.7,6.0)
29     CALL ENCLP(0)
30     RETURN
31     END
32 *****
33 SUBROUTINE TO CREATE GRAPH FOR ENDURANCE VELCCITY VS RADIUS
34 *****
35 *****
36 *****
37 *****
38 *****
39 *****
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99 *****
100 *****

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CALL DCT
CALL GRIC (1,2)
CALL RESET(,DOT)
CALL ENDCR(0)
-----
CALL PFYSOR(5,5,1.5)
CALL AREA2D (2,50,4,50)
CALL XNAME (,RADIUS OF MAIN ROTOR (,CHANGE),,100)
CALL YNAME (,ENDURANCE VELCCITY (,CHANGE),,100)
CALL GRAF (DMIN,SCALE,,DMAX,MINY,SCALE,,MAXY)
CALL CURVE (DRMR,DVFEND,324,0)
CALL DCT
CALL GRIC (1,2)
CALL ENDCR(0)
-----
CALL PFYSOR(1,5,1.5)
CALL AREA2C (6,50,4,70)
CALL HEADIN (,ENDURANCE VELOCITY VERSUS RADIUS$,32,1.4,3)
IF (K .NE. 1) GO TO 8
CALL HEADIN (,CHORD & ROTATIONAL VELCCITY HELD CONSTANT$,41,
0.8,3)
*
CALL HEADIN (,SOLICITY, TIP VELOCITY & ADVANCE RATIO$,38,0.8,4)
CALL HEADIN (,ALLOWED TO VARY WITH RADIUS$,27,0.8,4)
CALL MESSAGE (,SPEC RMR =$,100,7.4,6.5)
CALL REALNC (RMR(163),2,ABUT,,ABUT)
CALL MESSAGE (,CASE 1$,100,8.7,6.0)
IF (K .NE. 2) GO TO 10
CALL HEADIN (,CHORD, TIP VELOCITY & ADVANCE RATIO HELD CCNSTANT$,
48,0.8,4)
*
CALL HEADIN (,SOLICITY, ROTATIONAL VELOCITY$,29,0.8,4)
CALL HEADIN (,ALLOWED TO VARY WITH RADIUS$,27,0.8,4)
CALL MESSAGE (,SPEC RMR =$,100,7.4,6.5)
CALL REALNC (RMR(163),2,ABUT,,ABUT)
CALL MESSAGE (,CASE 2$,100,8.7,6.0)
IF (K .NE. 3) GO TO 12
CALL HEADIN (,SOLICITY & ROTATIONAL VELOCITY HELD CONSTANT$,
44,0.8,4)
*
CALL HEADIN (,CHORD, ADVANCE RATIO & TIP VELOCITY$,34,0.8,4)
CALL HEADIN (,ALLOWED TO VARY WITH RADIUS$,27,0.8,4)
CALL MESSAGE (,SPEC RMR =$,100,7.4,6.5)
CALL REALNC (RMR(163),2,ABUT,,ABUT)
CALL MESSAGE (,CASE 3$,100,8.7,6.0)
IF (K .NE. 4) GO TO 14
CALL HEADIN (,SOLICITY, ADVANCE RATIO & TIP VELOCITY HELD CONSTANT$,
51,0.8,4)
*
CALL HEADIN (,CHORD & ROTATIONAL VELOCITY$,27,0.8,4)
CALL HEADIN (,ALLOWED TO VARY WITH RADIUS$,27,0.8,4)
CALL MESSAGE (,SPEC RMR =$,100,7.4,6.5)

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PER13530
PER13540
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PER14020
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PER14290
PER14300
PER14310
PER14320
PER14330
PER14340
PER14350
PER14360
PER14370
PER14380
PER14390
PER14400

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CALL AREA2C (2.50,4.50)
CALL XNAME ('RADIUS OF MAIN ROTOR (FT)',$,100)
CALL YNAME ('MAXIMUM RANGE VELOCITY (KNOTS)',$,100)
CALL GRAF ('MINZ,$SCALE$,MAXZ,$SCALE$,MAX)
CALL CUFVE (RMR,VFRAN,324,-1)
CALL CCI
CALL GRID (1,2)
CALL RESET('DOT.')
CALL ENLCR(0)
*****
CALL PHYSOR(5.5,1.5)
CALL AREA2C (2.5,4.5)
CALL XNAME ('RADIUS OF MAIN ROTOR (% CHANGE)',$,100)
CALL YNAME ('MAXIMUM RANGE VELOCITY (% CHANGE)',$,100)
CALL GRAF ('DMIN,$SCALE$,DMAX,$SCALE$,MAX)
CALL CUFVE (DRMR,DVFRAN,324,-1)
CALL DCI
CALL GRID (1,2)
CALL ENLCR(0)
-----
CALL PHYSOR(1.5,1.5)
CALL AREA2C (6.50,4.70)
CALL HEADIN ('MAXIMUM RANGE VELOCITY VERSUS RADIUS CHANGE$',
43,1.4,4)
* IF (K.NE.1) GC TC 8
CALL HEADIN ('CHORD & ROTATIONAL VELOCITY HELD CONSTANT$',41,
0.8,3)
* CALL HEADIN ('SOLIDITY, TIP VELOCITY & ADVANCE RATIO$',38,0.8,4)
CALL HEADIN ('ALLOWED TO VARY WITH RADIUS$',27,0.8,4)
CALL MESSAGE ('SPEC RMR =$,100,7.4,6.5)
CALL REALNC (RMR(163),2,ABUT,ABUT)
CALL MESSAGE ('CASE 1$,100,8.7,6.0)
IF (K.NE.2) GC TO 10
CALL HEADIN ('CHORD,TIP VELOCITY & ADVANCE RATIO HELD CCNSTANT$',
48,3.8,4)
* CALL HEADIN ('SOLIDITY, ROTATIONAL VELOCITY$',29,0.8,4)
CALL HEADIN ('ALLOWED TO VARY WITH RADIUS$',27,0.8,4)
CALL MESSAGE ('SPEC RMR =$,100,7.4,6.5)
CALL REALNC (RMR(163),2,ABUT,ABUT)
CALL MESSAGE ('CASE 2$,100,8.7,6.0)
IF (K.NE.3) GC TC 12
CALL HEADIN ('SOLIDITY & ROTATIONAL VELOCITY HELD CCNSTANT$',
44,3.8,4)
* CALL HEADIN ('CHORD,ADVANCE RATIO & TIP VELOCITY$',34,0.8,4)
CALL HEADIN ('ALLOWED TO VARY WITH RADIUS$',27,0.8,4)
CALL MESSAGE ('SPEC RMR =$,100,7.4,6.5)
CALL REALNC (RMR(163),2,ABUT,ABUT)
CALL MESSAGE ('CASE 3$,100,8.7,6.0)

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8

10





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COMMON /W/ RCMAX(400), DRCMAX(400), VFRAN(400), DSEVAL(400), FDMERT(400),
* HCVALT(400), DHOVAL(400), SEVALT(400), DVFEND(400),
* DFMERT(400), VFEND(400), DVFEND(400),
CALL CCMPRS
CALL PACE(11,0,8.5)
CALL PFYSOR(1.5,1.5)
CALL AREA2D(2.50,4.50)
CALL XNAME(,RADIUS OF MAIN ROTOR (FT),$,100)
CALL YNAME(,MAXIMUM SERVICE CEILING (FT),$,100)
CALL GRAF(MINZ,SCALE,MAXZ,MIN,SCALE,MAX)
CALL CURVE(RMR,SEVALT,322,0)
CALL GCT
CALL GFIC(1,2)
CALL RESET(.DOT.)
CALL ENLGR(0)

C-----
CALL PFYSOR(5.5,1.5)
CALL AREA2D(2.50,4.50)
CALL XNAME(,RADIUS OF MAIN ROTOR (% CHANGE),$,100)
CALL YNAME(,MAXIMUM SERVICE CEILING (% CHANGE),$,100)
CALL GRAF(DMIN,SCALE,DMAX,MIN,SCALE,MAX)
CALL CURVE(DRMR,DSEVAL,324,0)
CALL GCT
CALL GRID(1,2)
CALL ENLGR(0)

C-----
CALL PFYSOR(1.5,1.5)
CALL AREA2D(6.50,4.70)
CALL HEADIN(,MAXIMUM SERVICE CEILING VERSUS RADIUS CHANGE$,
44,1.4,4)
* IF(K,NE,1)
CALL HEADIN(,GLTC 8
0.8,3)
* CALL HEADIN(,SOLIDITY, TIP VELOCITY & ADVANCE RATIO$,41,
38,0.8,4)
CALL HEADIN(,ALLOWED TO VARY WITH RADIUS$,27,0.8,4)
CALL MESSAGE(,SPEC RMR =$,100,7.4,6.5)
CALL REALNO(,RMR(163),2,ABUT,ABUT)
CALL MESSAGE(,CASE 1$,100,8.7,6.0)
IF(K,NE,2) GO TO 10
* CALL HEADIN(,CHORD,TIP VELOCITY & ADVANCE RATIO HELD CCNSTANT$,
48,0.8,4)
CALL HEADIN(,SOLIDITY, ROTATIONAL VELOCITY$,29,0.8,4)
CALL HEADIN(,ALLOWED TO VARY WITH RADIALS$,27,0.8,4)
CALL MESSAGE(,SPEC RMR =$,100,7.4,6.5)
CALL REALNO(,RMR(163),2,ABUT,ABUT)
CALL MESSAGE(,CASE 2$,100,8.7,6.0)
IF(K,NE,3) GO TO 12
* CALL HEADIN(,SOLIDITY & ROTATIONAL VELOCITY HELD CCNSTANT$,

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12      44,C.8,4) CHORD,ADVANCE RATIO & TIP VELCCITY$,34,0.8,4)
      CALL HEADIN (,ALLOWED TO VARY WITH RADIUS$,27,0.8,4)
      CALL MESSAG (,SPEC RMR =$,100,7.4,6.5)
      CALL REALNO (RMR(163),2,ABUT,ABUT)
      CALL MESSAG (,CASE 3$,100,8.7,6.0)
      IF (K.NE.4) GO TO 14
      CALL HEADIN (,SOLIDITY,ADVANCE RATIO & TIP VELOCITY HELD CONSTANT$,
      51,0.8,4)
      CALL HEADIN (,CHORD & ROTATIONAL VELCCITY$,27,0.8,4)
      CALL MESSAG (,ALLOWED TO VARY WITH RADIUS$,27,0.8,4)
      CALL MESSAG (,SPEC RMR =$,100,7.4,6.5)
      CALL REALNO (RMR(163),2,ABUT,ABUT)
      CALL MESSAG (,CASE 4$,100,8.7,6.0)
      CALL ENDPL(C)
      RETURN
      ENC
14      *****
      SUBROUTINE TO CREATE GRAPH OF FIGURE OF MERIT VS RADIUS
      *****
      SUBROUTINE GRAFLE
      IMPLICIT REAL (A-H,L-Z)
      COMMON /C/ RMR(400),I,J,K,DRMR(400),MINX,MAXX,MINY,MAXY,MINZ,
      * CMXZ,CMIN,CMAX,MINC,MAXC,MIN,MAX,MAXA,IANS,TEXT(200)
      COMMON /W/ RCMAX(400),DRCMAX(400),VFRAN(400),DVFRAN(400),
      * HCVALT(400),DHOVAL(400),SEVALT(400),DSEVAL(400),FMERT(400),
      * DFMER(400),VFEND(400),DVFEND(400)
      CALL CCMPRS
      CALL PACE (11.0,8.5)
      CALL PHYSOR (1.5,1.5)
      CALL AREA2D (2.50,4.50)
      CALL XNAME (,RADIUS OF MAIN ROTOR (FT)$,10C)
      CALL YNAME (,FIGURE OF MERIT$,100)
      CALL GRAF (MINZ,SCALE,MAXZ,SCALE,MAXB)
      CALL CURVE (RMR,FMERT,324,0)
      CALL DCT
      CALL GRID (1,2)
      CALL RESET (,DOT, )
      CALL ENGR(C)
      -----
      CALL PHYSOR (5.5,1.5)
      CALL AREA2D (2.50,4.50)
      CALL XNAME (,RADIUS OF MAIN ROTOR (2 CHANGE)$,100)
      CALL YNAME (,FIGURE OF MERIT (% CHANGE)$,100)
      CALL GRAF (CMIN,SCALE,CMAX,MINC,SCALE,MAXC)

```

```

PERI 7290
PERI 7300
PERI 7310
PERI 7320
PERI 7330
PERI 7340
PERI 7350
PERI 7360
PERI 7370
PERI 7380
PERI 7390
PERI 7400
PERI 7410
PERI 7420
PERI 7430
PERI 7440
PERI 7450
PERI 7460
PERI 7470
PERI 7480
PERI 7490
PERI 7500
PERI 7510
PERI 7520
PERI 7530
PERI 7540
PERI 7550
PERI 7560
PERI 7570
PERI 7580
PERI 7590
PERI 7600
PERI 7610
PERI 7620
PERI 7630
PERI 7640
PERI 7650
PERI 7660
PERI 7670
PERI 7680
PERI 7690
PERI 7700
PERI 7710
PERI 7720
PERI 7730
PERI 7740
PERI 7750
PERI 7760
PERI 7770

```



```

CALL CLFVE (DRMR,DFMERT,324,0)
CALL CCT
CALL GFIL (1,2)
CALL ENGR(0)
C-----
CALL PHYSOR(1,5,1,5)
CALL AREA2D (6,50,4,70)
CALL HEACIN (,FIGURE CF MERIT VERSUS RADIUS CHANGE$,
36,1,4,4)
* IF (K .NE. 1) GO TO 8
CALL HEACIN (,CHORD & ROTATIONAL VELOCITY HELD CONSTANT$,41,
0,8,3)
* CALL HEACIN (,SOLIDITY, TIP VELOCITY & ADVANCE RATIO$,38,0,8,4)
CALL HEACIN (,ALLOWED TO VARY WITH RADIUS$,27,0,8,4)
CALL MESSAGE (,SPEC RMR =$,100,7,4,6,5)
CALL REALNC (RMR(163),2,ABUT,ABUT)
CALL MESSAGE (,CASE 1$,100,8,7,6,0)
IF (K .NE. 2) GO TO 10
CALL HEACIN (,CHCRC,TIP VELOCITY & ADVANCE RATIO HELD CONSTANT$,
4,0,8,4)
* CALL HEACIN (,SOLIDITY, ROTATIONAL VELOCITY$,29,0,8,4)
CALL HEACIN (,ALLOWED TO VARY WITH RADIUS$,27,0,8,4)
CALL MESSAGE (,SPEC RMR =$,100,7,4,6,5)
CALL REALNC (RMR(163),2,ABUT,ABUT)
CALL MESSAGE (,CASE 2$,100,8,7,6,0)
IF (K .NE. 3) GO TO 12
CALL HEACIN (,SOLIDITY & ROTATIONAL VELOCITY HELD CONSTANT$,
4,0,8,4)
* CALL HEACIN (,CHORD, ADVANCE RATIO & TIP VELOCITY$,34,0,8,4)
CALL HEACIN (,ALLOWED TO VARY WITH RADIUS$,27,0,8,4)
CALL MESSAGE (,SPEC RMR =$,100,7,4,6,5)
CALL REALNC (RMR(163),2,ABUT,ABUT)
CALL MESSAGE (,CASE 3$,100,8,7,6,0)
IF (K .NE. 4) GO TO 14
CALL HEACIN (,SOLIDITY, ADVANCE RATIO & TIP VELOCITY HELD CONSTANT$,
51,0,8,4)
* CALL HEACIN (,CHORD & ROTATIONAL VELOCITY$,27,0,8,4)
CALL HEACIN (,ALLOWED TO VARY WITH RADIUS$,27,0,8,4)
CALL MESSAGE (,SPEC RMR =$,100,7,4,6,5)
CALL REALNC (RMR(163),2,ABUT,ABUT)
CALL MESSAGE (,CASE 4$,100,8,7,6,0)
CALL ENCLPL(C)
RETURN
END
=====
C SUBROUTINE RDINT --- INTERACTIVELY READS AN INTEGER REPLY
C INTO A FORTRAN PROGRAM. IF THE USER INADVERTENTLY ENTERS AN IMPROPER
PER17770
PER17780
PER17790
PER17800
PER17810
PER17820
PER17830
PER17840
PER17850
PER17860
PER17870
PER17880
PER17890
PER17900
PER17910
PER17920
PER17930
PER17940
PER17950
PER17960
PER17970
PER17980
PER17990
PER18000
PER18010
PER18020
PER18030
PER18040
PER18050
PER18060
PER18070
PER18080
PER18090
PER18100
PER18110
PER18120
PER18130
PER18140
PER18150
PER18160
PER18170
PER18180
PER18190
PER18200
PER18210
PER18220
PER18230
PER18240

```

```

C DATA CHARACTER THE S/R ISSUES A WARNING AND ALLOWS A RECOVERY.
C=====
C SUBROUTINE RJOINT ( IANS)
C INTEGER CCUNT
C-----
C COUNT=C
C CONTINUE
C COUNT=CCUNT+1
C IF (COUNT.LT.3) GO TO 20
C WRITE (5,60)
C GO TO 50
C CONTINUE
C READ (5,*,END=40,ERR=40) IANS
C IF (IANS) 40,40,30
C CONTINUE
C RETURN
C REWIND 5
C WRITE (5,70)
C GO TO 10
C CONTINUE
C STOP
C-----
C 60 FORMAT (//,5X,49HPROGRAM TERMINATION - TWO IMPROPER DATA ENTRIES
C 1)
C 70 FORMAT (1X,56HWARNING: IMPROPER DATA ENTRY ENTER A POSITIVE INTE
C 1GER.)
C END

```

```

=PER18250
PER18260
PER18270
PER18280
PER18290
PER18300
PER18310
PER18320
PER18330
PER18340
PER18350
PER18360
PER18370
PER18380
PER18390
PER18400
PER18410
PER18420
PER18430
PER18440
PER18450
PER18460
PER18470
PER18480
PER18490
PER18500
PER18510
PER18520

```

AD-A151 488

PRELIMINARY HELICOPTER DESIGN DECISION MAKING BASED ON  
FLIGHT PERFORMANCE FACTORS(U) NAVAL POSTGRADUATE SCHOOL  
MONTEREY CA P V ADANCIK SEP 84

2/2

UNCLASSIFIED

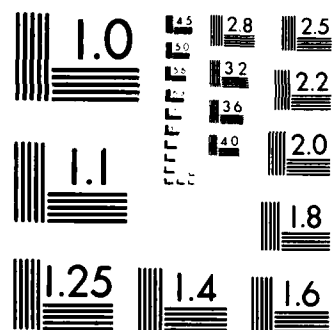
F/G 6/3

NL

END

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DTIC



MICROCOPY RESOLUTION TEST CHART  
NATIONAL BUREAU OF STANDARDS 1963-A

## LIST OF REFERENCES

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2. Layton, Professor Donald M., Helicopter Performance, Naval Postgraduate School, Monterey California, 1983.
3. Layton, Professor Donald M., AE 4306 Design Design Manual, Naval Postgraduate School, Monterey California, 1983.

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